

Average Year Results	Junction 1	Junction 2	Junction 3	Total	Pollutant load	Ave daily concen.
					kg/ha/yr	mg/L
Total Nitrogen (kg/yr)	596	2730	1420	4746	14.03	1.14
Gross Pollutants (Kg/yr)	39.1	680	202	921.1	2.72	n/a

The wetlands reduce annual TSS loads by 66 %, TP loads by 34 % and TN loads by 8%. Gross pollutants are greatly reduced by around 98%, however the other pollutants still exceeded the requirements of Council as shown below in Table 3.18.

Table 3-18: Comparison of wetland case performance against TSC WQO

Pollutant	Wetland Outflow	TSC WQO	Exceedance factor
	(kg/ ha)	(kg/ ha)	
Total Suspended Solids	342.7	300	1.1
Total Phosphorous	1.66	1.65	1.0
Total Nitrogen	14.03	13	1.1

The results indicate that wetlands alone will provide a good level of treatment, however additional measures to form a stormwater treatment train will be required to provide sufficient removal of stormwater pollutants.

The wetlands have been sized using the TSC guidelines. A review by Dr Graham Jenkins indicated that the inlet zone of the wetland sized using the guidelines are reasonably large. In MUSIC, the open water zone or sedimentation basin of a constructed wetland is modelled as an inlet pond. Typically, the aim of the sedimentation basin is to capture sediment particles approximately 125 µm in size during a three month ARI design storm. The settling velocity of a particle of this size is approximately 0.012 m/s. The surface area of the wetlands can be calculated by dividing the design flow by the settling velocity, which in this case would indicate much smaller inlet ponds than calculated using the TSC guidelines. The larger inlet ponds may be used to mitigate the increase in peak flows resulting from urbanisation. Overflow weirs could be designed to allow flows greater than the wetland capacity to be bypassed with inlet pipes discharging the design storm through the wetland. The required sizes of detention basins have been estimated in section 3.4.4. Buffers will be required around the wetlands for maintenance and should be allowed for in any preliminary planning. The inlet ponds have been modelled as per the TSC guidelines with their characteristics provided below in Table 3.19.

Table 3-19 Wetland sizes

Sub-catchment	Inlet Pond		Macrophyte Zone		
	Surface Area (ha)	Volume (m3)	Surface Area (ha)	Extended Detention depth (m)	Permanent Pool Volume (m3)
1	1.2	18525	1.2	0.5	8645
2	5.1	75700	5.1	0.5	35350
3	2.2	32625	2.2	0.5	15225

3.4.3.7 Mitigation option 2 – WSUD

The use of water sensitive urban design philosophies of vegetated swales and bio-retention trenches was adopted for the second case. It was assumed that all allotments would fall to a vegetated swale that discharged to a bio-retention trench. The adopted parameters for both treatment measures were estimated as there is no current lot layout to calculate the actual treatment train lengths. It was assumed that the roads would run generally parallel with the contours rather than across them.

The adopted parameters are provided below in Table 3.20. It is suggested that these criteria together with Tweed Shire Council's development guidelines (DCP16 Subdivision Manual - Section 4.2.3 Stormwater runoff, drainage, waterways and flooding; Development Design Specification D5 Stormwater Drainage Design; and Development Design Specification D7 Stormwater Quality) be adopted for future development.

Table 3-20: Grassed swale and bio-retention design parameters

Design Parameter - Grassed Swale		Design Parameters Bio-retention trench	
Length (m)	continuous	Length (m)	70m per ha
Slope (%)	2	Slope (%)	Flat
Base width (m)	1.5	Base width (m)	1.5
Depth (m)	0.5	Extended Detention Depth (m)	0.5
Vegetation height (mm)	100	Filter Depth (m)	1
Side slopes (1 in x)	4	Side slopes (1 in x)	4

The MUSIC model assumes that the treatment measures are in series downstream of the source nodes, however vegetated swales and bio-retention trenches are usually distributed throughout the catchment receiving distributed flows rather than a plug flow. An Excel spreadsheet for a small 1 ha catchment consisting of 10 allotments (1 ha in area allowing for road reserve and open space) was produced that allowed for individual allotment flows to enter a 200 m long swale fronting each allotment. The model cumulated flow from each individual block and calculated the various detention times each allotment flow would receive. The model showed that flow from the upper allotment would receive a detention time of over nine minutes, the middle allotment over five minutes, and the final allotment runoff would only travel in the swale for over one minute for the three month ARI flow. Overall, the runoff from all 10 allotments would receive good treatment with an average treatment time of over five minutes. As MUSIC models swales at the end of the catchment, not throughout the catchment, the equivalent swale configuration at the end of the 10 allotments was estimated using a similar Excel spreadsheet. The model showed that a swale length of 80 m would provide just over five minutes of retention time for the entire flow. This methodology was then adopted for all vegetated swales within the MUSIC model as it was assumed that the retention time is the main parameter of swale pollutant removal.

The scale of the catchments in the MUSIC model is much greater than 1 ha, therefore the scale of the swale had to be increased as the catchment area increased. As flow depth, velocity and retention time are the key parameters for swales, it was assumed that a doubling in catchment area would require a doubling in base width of the swale to approximate a more realistic flow depth, rather than doubling the length of the swale. Similar Excel spreadsheets were used to verify this assumption and a peer review by Dr Graham A Jenkins confirmed that this approach, while not 100 % correct (as the response is not linear), was the best approach to model a distributed swale network for large catchments.

The bio-filtration treatment processes are dependant on filter depth, filter media, surface area and extended detention depth. The surface area was therefore scaled up from the 1 ha catchment model which assumed a base width of 1.5 m for a length of 80 m. It was assumed that sand would be used as the filter media with an equivalent particle size of 0.7 mm and a saturated hydraulic conductivity of 360 mm/hr.

The MUSIC model was used to evaluate the expected performance of the vegetated swales and bio-retention systems and the results of the modelling are provided below in Table 3.21.

Table 3-21: Developed Mitigated Case WSUD – Pollutant Loads and Annual Flow

Average Year Results	Junction 1	Junction 2	Junction 3	Total	Pollutant load	Ave daily concen.
					kg/ha/yr	mg/L
Flow (ML/yr)	429	2230	993	3652	n/a	n/a
Total Suspended Solids (kg/yr)	11900	59000	27000	97900	289.5	2.9
Total Phosphorous (kg/yr)	38.3	194	90.2	322.5	0.95	0.03
Total Nitrogen (kg/yr)	229	1360	626	2215	6.55	0.30
Gross Pollutants (Kg/yr)	0	0	0	0	0.00	n/a

The results assume that swales will be continuous throughout the model and that they will have a grade of 2%. Any deviation from this will result in different pollutant removal efficiencies.

The MUSIC model results indicate that the WSUD treatment measures adopted will meet TSC's required annual pollutant guidelines. TSS is reduced by 71% from the developed unmitigated case, while TP and TN are reduced by 62% and 57% respectively. The model indicates that gross pollutants are completely removed by the treatment system. Pollutants could be reduced further by lengthening vegetated swales and increasing the surface area and depth of bio-retention, however the steep nature of the site will limit the effective length of both measures. The adopted lengths have been estimated by preparing a possible lot layout for one of the sub-catchments and estimating appropriate lengths.

3.4.3.8 Mitigation Option 3 – WSUD including rainwater tanks

Rainwater tanks were added to the WSUD case to observe their impact on pollutant loads. The MUSIC model does not include the option of adding rainwater tanks, however they were simulated by adding the MUSIC pond treatments. It was assumed that each allotment would have a 7.5 kL tank approximately 2 m high. The tanks were assumed to have a low flow bypass of 1l/s to allow for the bypass of first flush. Once the tanks are full, any excess water will overtop the storage and be directed towards the swales and bio-retention trenches. Recent studies by the Gold Coast City Council have indicated that the average water use per allotment is 693 L/ET.day (Gold Coast Water, 2003). The same study concluded that rainwater could be used to supplement between 30% (external use only) to 90% (all water use except kitchen use). This study has assumed that 75% of daily household water demand could be supplied by rainwater, if available. The break-up of this is provided in the table below.

Table 3-22: Household water use

House hold use	% of total household use	Daily Water volume (litres)	Volume Adopted for Rainwater demand (litres)
Kitchen	10	69	0
Bathrooms	15	104	0
Laundry	15	104	104
Hot water	15	104	104
Toilets	15	104	104
External	30	208	208
TOTAL	100	693	520

It should be noted although the goal is to use rainwater for 75% of the daily household water supply, rainfall patterns and tank sizing may limit the available supply to much less than 75%.

It was assumed that each allotment had a daily demand of 520 L from the rainwater tanks and that each allotment has a roof area of 300 m². An additional source node was created to represent the roof area and typical roof pollutant loads were adopted by research from Duncan 1999. The TSC urban source node was amended to account for the loss of roof area with both the runoff and pollutant characteristics being amended. A check of both runoff volumes and the pollutant characteristics was undertaken to ensure that the separated source nodes produce the same characteristics as the TSC urban source node. The results of the MUSIC model are provided below.

Table 3-23: Developed Mitigated Case WSUD with rainwater tanks – Pollutant Loads and Annual Flow

Average Year Results	Junction 1	Junction 2	Junction 3	Total	Pollutant load	Ave daily concen.
					kg/ha/yr	mg/L
Flow (ML/yr)	420	2110	938	3468	n/a	n/a
Total Suspended Solids (kg/yr)	11700	57200	26100	95000	280.9	2.9
Total Phosphorous (kg/yr)	37.4	187	86.8	311.2	0.92	0.03
Total Nitrogen (kg/yr)	221	1300	598	2119	6.27	0.30
Gross Pollutants (Kg/yr)	0	0	0	0	0.00	n/a

The MUSIC model results indicate that the WSUD incorporating rainwater tanks will provide a small improvement to water quality. TSS is reduced by 72% from the developed unmitigated case, while TP and TN are reduced by 64% and 59% respectively. It would be expected that the addition of rainwater tanks would provide a greater benefit than a reduction of just 15% in annual flow volumes. This may be due to the rainfall pattern from the adopted average year which consists of large rainfall events dispersed throughout the year. A long term daily balance could be undertaken to analyse the change in flow conditions over a much longer period to determine if a greater supply of water from rainwater tanks is possible.

The rainwater tanks will also provide the benefit of reducing the demand on potable supplies. The Gold Coast City Council has estimated that domestic potable water demand could be reduced by up to 50% after the adoption of suitably sized rainwater tanks (Gold Coast Water, 2003). Measures should be in place to ensure that the maximum volume of rainwater is captured and stored for household use. The ability to capture the maximum possible roof area, installing large enough tanks to store water between dry periods, location of tanks (surface or buried tanks), and the ability to pump water to various areas of the house should be investigated to optimise rainwater tank performance. Manufacturers of rainwater tanks and pump systems should be consulted to provide guidance on the practical applications of suitable systems.

3.4.3.9 Mitigation option 4 – Treatment Train Approach

The MUSIC model indicates that an approach adopting grassed swales and biofiltration measures can reduce pollutants sufficiently to meet the TSC annual pollutant load requirements. This option was based on the criteria that grassed swales and biofiltration would be suitable for the entire site, based on an initial review of a potential lot layout. Best practice suggests that a treatment train approach would be appropriate to enhance further pollutant removal and provide a “redundancy” should a particular measure fail. The WSUD case with rainwater tanks was amended to include the wetlands previously modelled to provide a treatment train for the catchment. The design criteria discussed previously for each individual measure was adopted for this case. The results of the MUSIC model are provided below in Table 3.24.

Table 3-24: Developed Mitigated Case Treatment Train (Wetlands, WSUD with rainwater tanks) – Pollutant Loads and Annual Flow

Average Year Results	Junction 1	Junction 2	Junction 3	Total	Pollutant load	Ave daily concen.
					kg/ha/yr	mg/L
Flow (ML/yr)	395	2010	895	3300	n/a	n/a
Total Suspended Solids (kg/yr)	9280	49200	21300	79780	235.9	5.8
Total Phosphorous (kg/yr)	55.8	286	128	469.8	1.39	0.08
Total Nitrogen (kg/yr)	423	2180	1090	3693	10.92	0.96
Gross Pollutants (Kg/yr)	0	0	0	0	0.00	n/a

The MUSIC model results indicate that the treatment train approach provides the greatest level of TSS reduction of 77% from the developed unmitigated case. TP and TN reductions are still in-line with the requirements of TSC, however the addition of the wetlands provides a slight increase in both from Option 3. This increase is due to the MUSIC model default parameter of C* which equates to the minimum concentration that can be discharged by the treatment device, such as a wetland. Any increase in wetland size, detention time etc will not provide any reduction of pollutants below this level.

A review of site constraints has indicated that the available area for each wetland is around 50% of the area required for wetlands as per the TSC design guidelines. The inlet pond has therefore been reduced to the size suggested by Dr Jenkins which is based on the settling velocity of a sediment particles approximately 125 µm in size during a three month ARI design storm.

A separate MUSIC model was constructed with the following inlet pond volumes provided below:

- Wetland 1 – 434 m³;
- Wetland 2 – 1000 m³; and
- Wetland 3 – 563 m³.

The results of the MUSIC model are provided below.

Table 3-25: Smaller Inlet pond wetlands – pollutant loads and annual flow

Average Year Results	Junction 1	Junction 2	Junction 3	Total	Pollutant load	Ave daily concen.
					kg/ha/yr	mg/L
Flow (ML/yr)	395	2010	895	3300	n/a	n/a
Total Suspended Solids (kg/yr)	8060	40900	18500	67460	199.5	5.6
Total Phosphorous (kg/yr)	42.6	219	99.1	360.7	1.07	0.08
Total Nitrogen (kg/yr)	321	1690	870	2881	8.52	0.95
Gross Pollutants (Kg/yr)	0	0	0	0	0.00	

The results indicate that the wetlands with smaller inlet ponds provide better treatment than the larger ponds with a reduction of annual TSS loads by 80 %, TP loads by 58 % and TN loads by 44%. This may indicate that the larger pond surface areas are redundant and do not contribute to any greater removal of stormwater pollutants.

It is recommended that the mitigation option 4, the treatment train approach, be adopted for the Tweed Area E development. The adoption of a range of best practice stormwater treatment measures that includes wetlands will provide additional water quality treatment should site constraints prevent any section of the system from performing to expectations. The addition of wetlands and rainwater tanks will provide additional benefits such as the attenuation of more frequent events and assist in limiting the impact of increased levels of imperviousness through the new development.

3.4.3.10 Cost estimate

Cost estimates for the three water quality infrastructure cases are provided in Table 3.26 below. The three cases investigated include:

- wetlands;
- grass swales and bio retention; and
- grass swales, bio retention and rainwater tanks.

The cost of the wetlands is high as the inlet ponds surfaces areas are large, as discussed previously.

Table 3-26: Cost estimate summary

	Capital Cost	Maintenance Cost per year
Wetlands		
Catchment 1 – 49ha	\$735,000	\$15,000
Catchment 2 – 202ha	\$3,030,000	\$60,000
Catchment 3 – 87ha	\$1,305,000	\$26,000
Total – Option 1	\$5,070,000	\$101,000
Grass Swales & Bio Retention		
Grass Swales	\$1,010,000	\$45,000
Bio-retention	\$945,000	\$60,000
Total – Option 2	\$1,955,000	\$105,000
Grass Swales & Bio Retention & Rainwater Tanks		
Grass Swales	\$1,010,000	\$45,000
Bio-retention	\$945,000	\$60,000
Rainwater Tanks	\$8,400,000	\$300,000
Total – Option 3	\$10,355,000	\$405,000
Treatment Train using all measures		
Grass Swales	\$1,010,000	\$45,000
Bio-retention	\$945,000	\$60,000
Rainwater Tanks	\$8,400,000	\$300,000
Wetlands	\$5,070,000	\$100,000
Total – Option 4	\$15,425,000	\$505,000
	(\$7,025,000 not incl. rain tanks)	(\$205,000 not incl. rain tanks)

Wetland costs are based on \$15,000/ha of catchment area reporting to the wetland.

Grass swale costs are based on \$46/m, with 65 m of swale allowed for per hectare.

Bio-retention costs are based on \$80/m, with 35 m of bio-retention swale allowed for per hectare. Bio-retention costs also allow for a grass swale on top of each bio-retention trench.

Rainwater tank costs allow for one tank per allotment, assuming 10 allotments per hectare. Rainwater tanks are based on \$3000 per 7.5 kL tank and pump.

Maintenance costs are based on the following:

- wetlands systems \$6000/ha of wetland/year;
- rainwater tanks and gross pollutant traps 3% of the capital per year;
- swales \$3/m/year; and
- bio-retention \$5/m/year.

No additional allowance has been made for asset replacement after a predetermined time.

3.4.3.11 Additional Pollutants

The WQO's identified in the EPA interim guidelines include parameters for the protection of aquatic ecosystems, shellfish production and recreational activities. These values include

parameters such as faecal coliforms, pH, turbidity and dissolved oxygen. The MUSIC program was used to identify the water quality impacts from catchment development and evaluate the performance of potential stormwater quality treatment measures. The default MUSIC pollutants do not include these parameters; however they could be modelled if sufficient statistical data existed. Discussions with TSC officers have indicated that this data is currently not available. PB has reviewed research undertaken by the CRC for Catchment Hydrology to identify the likely concentrations of these additional pollutants from a typical urban catchment in order to assess their likely impact on downstream water quality.

Table 3.27 highlights the expected concentration and the required concentration to protect the desired value as presented in the NSW EPA interim guidelines. Where different environmental values have objectives for the same pollutant, the more stringent criteria has been identified, eg. the water quality objectives for primary contact recreation have been adopted over those for secondary contact recreation.

Table 3-27: Additional water quality objectives

Indicator	WQO	Expected Pollutant value	Environmental Value
Chlorophyll-a	1-10µg/L		Aquatic ecosystem
Dissolved Oxygen	>6mg/L or 80-90 % saturation over a 24 hour period		Aquatic ecosystem
pH	5.0-9.0	6.8	Aquatic ecosystem, Primary contact recreation
Chemical contaminants	Free from chemicals or pollutants that are either toxic to humans, animals, plants and other organisms or irritating to the skin or mucus membranes Refer to ANZECC (1992) guidelines for chemical contaminants and tainting substances.		Aquatic ecosystem, Primary contact recreation. Aquatic Foods (cooked)
Surface films and debris	Oils and petrochemical films should not be noticeable as a visible film nor detected by odour. Free from floating debris and litter.		Primary contact recreation, Visual Amenity
Faecal coliforms	Median over bathing season < 150 faecal coliforms per 100mL, with 4 out of 5 samples < 600/100mL Median bacterial concentration < 14MPN/100mL; 10 % of samples > 43 MPN/100mL NSW SQAP media faecal coliform level of 14 faecal coliforms/100mL	25,000/100ml	Primary contact recreation Aquatic Foods (cooked)
Turbidity	Approximately 5 NTU	70 NTU	Aquatic Ecosystems, Primary contact

Indicator	WQO	Expected Pollutant value	Environmental Value
			recreation
Algae and blue green algae	No guidelines for aquatic foods, however limit blue green algae which may contain toxins Primary contact recreation < 15 000 cells/mL	Dependant on Nutrient bioavailability	Aquatic Foods (cooked), Primary contact recreation
Enterococci	<35 /100mL		Primary contact recreation
Protozoans	Pathogenic free-living protozoans should be absent		Primary contact recreation
Temperature	15-35 deg C < 2 deg increase		Primary contact recreation, Aquatic ecosystems
Visual clarity and colour	< 20% reduction in visual clarity Waters deeper than 50% euphotic depth – depth should not change by more than 10%. Waters shallower than 50% of euphotic depth max reduction in light at the sediment bed should not exceed 20% < 10 point change on Munsell Scale <50% change in natural reflectance		Aquatic ecosystems, Visual Amenity
Nuisance organisms	Macrophytes, phytoplankton scums, filamentous algal mats, blue-green algae, sewage fungus and leeches should not be present in unsightly amounts		Visual Amenity
Salinity	<1500 uS/cm		Aquatic ecosystems

The following is a summary of each physico-chemical indicator for the environmental values significant to Tweed Area E:

- primary recreation;
- secondary recreation;
- visual amenity;
- aquatic ecosystems; and
- aquatic foods (shell fish).

Primary recreational contact relates to activities such as swimming, bathing and other direct water-contact sports and the water quality objectives require that the water should be sufficiently free from faecal contamination, pathogenic organisms and other hazards such as poor visibility or toxic chemicals to protect the health and safety of the user.

Secondary contact activities such as boating and fishing relate to usage where there is less body contact with the water and need to incorporate excessive growth of algae and other plants, and floating or submerged debris which could injure skiers or damage boating vessels.

Aquatic ecosystems comprise the plant, animal and microbial communities that live in water and the physical environment and climate regime with which they interact. The guidelines

required to protect aquatic ecosystems are often the most stringent, and specifically in this case because of the downstream shellfish culture and harvesting.

Surface waters used for visual recreational use (no-contact activity) should not be altered in any way that reduces their ability to support aesthetically valuable flora and fauna. Visual amenity is directly related to each of the above environmental values and can be improved by protecting the ecosystems and improving stormwater quality management (EPA interim guidelines).

Turbidity

Turbidity is a pollutant that impacts primary recreation and aquatic ecosystems environmental values. The turbidity of water is caused by the presence of suspended particulate and colloidal matter consisting of suspended clay, silt, phytoplankton and detritus. Turbidity depends mostly on particle size, composition and particle concentration and the main source is usually from fine particulates, 0.125 mm and below (Fletcher et al, 2003).

Impacts

Water clarity is a major determinant of the condition and productivity of an aquatic system, and of the quality of water for primary recreation. Increased turbidity can change an ecosystem significantly, reducing the light available for photosynthesis.

Turbidity caused by suspended sediment can smother benthic organisms and habitats, and cause mechanical and abrasive impairment to the gills of fish and crustaceans. Suspended sediment also transports contaminants (particulate nutrients, metals and other potential toxicants), promotes the growth of pathogens and waterborne diseases, makes marine pests difficult to detect and can lead to dissolved oxygen depletion in the water column if it is caused by particulate organic matter.

Potential Sources

Tweed Area E is primarily a residential development and the main source of suspended particulate matter is from diffuse land runoff due to soil erosion in the upstream catchment. Suspended particulate matter could arise from point sources such as sewage outfalls and stormwater drains.

Management Practices

Useful structural stormwater treatment measures for turbidity are given below:

- grass swales;
- sand filters;
- porous pavements; and
- constructed wetlands.

These appropriate treatment measures are able to retain particles down to 0.45 µm (NSW EPA, 1997) which is expected to reduce turbidity levels. Optimum structural treatment methods include filters and porous pavements because they target the smaller particle sizes (GCCC, 2002). Constraints to sand filter treatment performance includes hydraulic head loss limitation and high sediment input, similarly constraints for porous pavements include, steep catchment slopes, high water tables, shallow bedrock and land availability.

Managing the construction and operational phases of the development at the source is a positive option to assist in reaching guideline turbidity values. Source management options include:

- Minimising stormwater runoff across construction sites and areas of roadwork to prevent sediment washing downstream.
- Provision of a buffer zone with a mixture of native plants to filter runoff from disturbed slopes, trapping pollutants and stabilizing gully banks, preventing bank erosion. These plants will also provide a natural riparian ecosystem.
- community education to encourage increased planting and maintenance of native vegetation on properties and including information about the importance of buffer zones and riparian vegetation along creeks.

Appendix F shows the pollutant reduction efficiencies for a range of structural stormwater management practices.

Algal Blooms

The environmental values that are directly affected by algal blooms are cooked shellfish and primary recreation. Algal blooms occur naturally with phytoplankton or micro-algae providing food for aquatic organisms. Harmful algal species are usually naturally occurring algae that reach high enough concentrations to be a nuisance. Harmful algal blooms can be divided into three groups:

1. group one (some cyanobacteria, diatoms and macroalgae) – when these species occur in dense blooms, they can cause fish and invertebrate kills as dissolved oxygen is consumed when the bloom decomposes;
2. group two (toxic cyanobacteria and dinoflagellates) – harmful algal species that produce potent toxins and can cause illness or death in grazers which may impact species further up the food chain due to the effects of bioaccumulation; and
3. group three (some diatoms, dinoflagellates and raphidophytes) – species that are not toxic, but that have physical attributes such as spines which can irritate and damage gills and tissues of fish.

Impacts

Harmful algal species can be composed of species that are toxic and irritate the skin of humans (public health nuisances) or be toxic to fish and other aquatic life. Blooms give rise to large fluctuations in water column dissolved oxygen concentrations and pH, and only species with broad dissolved oxygen and pH tolerances can survive. In addition, when the microalgae decay it releases waste products and bioavailable nitrogen, produces offensive odours and consumes large amounts of dissolved oxygen. Aquaculture production can be severely impacted by the presence of algal blooms, both from direct mortality of fish and shellfish due to reduced dissolved oxygen availability and the potential bioaccumulation of toxins if filter feeding organisms are being grown.

Potential Sources

Blooms are most common if warm, calm and stratified conditions occur after rainfall events in waterbodies and estuaries that are subject to elevated nutrient loads. If nutrient loads within the Tweed Area E development are high and there are no natural systems in place for dilution, then algal blooms could occur.

Management Practices

PB developed a water quality pollutant export model to generate pollutant loads and event mean concentrations for Total Phosphorus and Total Nitrogen. The structural stormwater treatment measures proposed to assist in the mitigation of high nutrient levels were:

- wetlands;
- at source vegetated swales and bio-retention trenches; and
- rainwater tanks together with at source vegetated swales and bio-retention trenches.

Because of the direct relation to nutrient loading, algal blooms are not expected to be a problem for the Tweed Area E development if the above measures are implemented and successful in mitigating high nutrient loads.

Further management options for high nutrient loading include source measures such as reducing stormwater runoff and rehabilitating riparian zones to assimilate nutrients (Cranmer et al, 2001). Some possible alternatives to structural treatment measures are given below:

- encourage properties to use native vegetation along creeks and elsewhere on private property to naturally filter organic material;
- educate and encourage residents to adopt stormwater wise management practices to reduce nutrient generation at the source;
- rehabilitate riparian zones to act as a natural trap for sediments and nutrients; and
- encourage residents to control animal wastes and fertilizer use through education via pamphlets and signs in parks and other recreational areas.

Dissolved Oxygen

Measures of dissolved oxygen (DO) refer to the amount of oxygen contained in water, and define the living conditions for oxygen-requiring (aerobic) aquatic organisms. DO concentrations reflect equilibrium between oxygen-producing processes (e.g. photosynthesis) and oxygen consuming processes (e.g. aerobic respiration, nitrification). The dissolved oxygen concentration in a waterbody is highly dependant on temperature, salinity, biological activity (microbial, primary production) and rate of transfer from the atmosphere.

Impacts

Low DO concentrations can result in adverse effects on many aquatic organisms (e.g. fish, invertebrates and microorganisms) which depend upon oxygen for their efficient functioning. Most aquatic organisms require oxygen in specified concentration ranges for respiration and efficient metabolism, and DO concentration changes to above or below this range can have adverse physiological effects. Even short-lived anoxic conditions (DO concentrations near zero) or hypoxic conditions (DO concentrations < 2.0 mg/L) can cause major kills of aquatic organisms (AGGA et al 2003). Exposure to low oxygen concentrations can have an immune suppression effect on fish which can elevate their susceptibility to diseases for several years. Moreover, the toxicity of many toxicants (lead, zinc, copper, cyanide, ammonia, hydrogen sulfide and pentachlophenol) can double when DO is reduced from 10 to 5 mg/L (NSW EPA, 2003). If dissolved oxygen becomes depleted in bottom waters (or sediment), nitrification, and therefore denitrification, may be terminated, and nutrients may be released from the sediment to the water column which can give rise to or support algal blooms.

Potential Sources

Dissolved oxygen levels are primarily dictated by nutrient levels in the water. Nutrient enrichment stimulates plant and algal growth (and algal blooms as discussed previously) and often results in a mass influx of particulate organic matter to the sediments (eutrophication). The decomposition of this organic matter by aerobic microorganisms leads to a rapid acceleration of oxygen consumption, and potential depletion of oxygen in bottom waters. Increased human activity will be the main source of nutrient loads in Tweed Area E in addition to eroded soils and aquaculture. In Australia, nitrogen and phosphorus export in waterways increases with the extent of catchment cleared.

Management Practices

The amount of dissolved oxygen is related primarily to the discharge of nutrients into the Tweed Area E waterways. As described in the suggested management practices of algal blooms, low dissolved oxygen should not be an issue for the development if nutrient loads are successfully managed as water quality modelling demonstrated. Structural stormwater treatment measures have been recommended to help mitigate high nutrient loading and indirectly mitigate both algal bloom and dissolved oxygen pollutants.

At source management options such as community education on stormwater management and riparian habitat rehabilitation as described for both nutrient loading and algal blooms will be effective in mitigating dissolved oxygen problems.

Chlorophyll a

Chlorophyll a (chl a) is a physico-chemical indicator for aquatic ecosystem health. Chlorophyll a is a green pigment found in plants. It absorbs sunlight and converts it to sugar during photosynthesis. Chl a in the water indicates that plants, algae or cyanobacteria are actually growing and that appropriate management action should be taken to identify the species. Chl a can be used as a non-specific indicator of the trophic status (level of pollution) of a water body.

Impacts

High chlorophyll concentrations can lead to excessive water column productivity and contribute to high amounts of easily decomposed organic matter to the sediments. Photosynthetic production and subsequent decomposition of algal biomass can increase the diurnal amplitude of water column pH and dissolved oxygen fluctuations, and in some cases may lead to anoxic and hypoxic events. The above changes can translate into an overall reduction in animal and plant species diversity.

Potential Sources

Chlorophyll a concentrations can be an alternative indicator of nutrient pollution. It is natural for chlorophyll a levels to fluctuate over time. Chlorophyll a concentrations are often higher after rainfall, particularly if the rain has flushed nutrients into the water. Higher chl a levels are common during the summer months when water temperatures and light levels are high because these conditions lead to greater phytoplankton numbers. Nutrient loading into the waterways will directly affect the chlorophyll a levels. Changes to systems which decrease (e.g. construction of canal estates) or increase (e.g. breakwaters, training water, and dredging) flushing rates influence chlorophyll a concentrations because flushing dilutes nutrients and moves them away from plants, making them less available. Conversely, slow moving or stagnant waters let nutrients increase and cell numbers grow.

Management Practices

The management strategies that have been recommended for nutrient loading in the Tweed Area E development will assist in mitigating chlorophyll a levels. Investigation of construction practices in the residential area is needed to ensure that the aquatic ecosystem and flushing system of the waterway is not adversely affected.

Faecal Coliforms

Faecal coliforms are indicators of disturbance to environmental values such as shellfish and primary recreation and are used as an indicator of faecal contamination of water. Faecal coliforms are bacteria and are a subset of total coliforms, and are more closely associated with faecal contamination. *Escherichia coli* (*E. coli*) is a member of this group, and is specifically of faecal origin (Duncan, 1999). Faecal coliforms are used to indicate the presence of viruses in the aquatic food and ecosystems because the viruses of concern to human health are derived mainly from sewage, *E. coli* and other faecal coliforms.

Impacts

Primary Recreation – faecal coliform is an indicator for detection of pathogens in fresh and marine waters. There is a long international experience of disease outbreaks associated with bathing areas contaminated with pathogens such as salmonellae, shigellae, enteropathogenic *Escherichia coli* and infectious hepatitis (ANZECC, 2000). Generally, the most common types of diseases that have been associated with swimming areas are eye, ear, nose and throat infections, skin diseases and gastrointestinal disorders.

Shellfish (cooked) – there are a number of biological contaminants which can affect human consumers of aquatic foods, including bacteria, viruses, parasites and micro-algae. Filter-feeding shellfish (bivalves) can concentrate these potential contaminants to levels higher than that in the water source. Shellfish are considered to be a higher risk for consumers of aquatic foods (ANZECC, 2000).

Potential Sources

Faecal coliform counts from residential areas are typically ten times as large as those from other types of high urban land use (Duncan, 1999). Possible causes include:

- sewer overflows — to release to land any sewage flow blockages resulting from pump failure and other disturbances; and
- household pets and native animals — faecal contamination around parklands and lakes, runoff into waterbodies.

Management Practices

Useful structural stormwater treatment measures to prevent contamination from faecal coliforms are given below:

- filter strips;
- grass swales;
- sand filters;
- infiltration trench/basin;
- porous pavements;
- extended detention basin; and
- constructed wetlands.

Porous pavements, filter strips, grass swales and constructed wetlands are the optimum treatment methods (BCC, 2000), however site constraints must be considered before adopting any structural treatment measure.

Preventing faecal coliforms at the source is a positive option to assist in reaching guideline values. Source management options include:

- encouragement of responsible pet ownership, e.g. doggie bags for pet faeces located at walkways and parks; and
- signs highlighting regulations and fines signs for pet walkways, parks and lakes to dispose correctly of domestic animal faeces.

Appendix F shows the pollutant reduction efficiencies for the faecal coliform management practices.

Salinity

Salinity or electrical conductivity are measures of the total concentration of inorganic ions (salts) in estuarine and marine waters, with ocean waters having a salinity around 35 parts per thousand (ppt) (AGGA et al, 2003). EC is used to measure the total ion concentration in fresh and brackish waters. Measures of salinity can indicate whether the chemical nature of aquatic ecosystems is being altered and provides a warning of the potential loss of native biota.

Impacts

Most aquatic organisms function optimally within a narrow range of salinity. Salinity changes may affect aquatic organisms in two ways:

- direct toxicity through physiological changes (particularly osmoregulation) – both increases and decreases in salinity can have adverse effects; and
- indirectly by modifying the species composition of the ecosystem and affecting species that provide food or refuge.

While freshwater biota are most vulnerable to increased salinity, marine and estuarine biota are equally susceptible to decreased salinity. The development of salinity guidelines is complicated because of the uncertainty of whether discharges of either highly saline water or freshwater is likely to substantially change the existing (or desired) salinity regime in the system. Trigger values for naturally saline wetlands or streams, and similarly for systems with naturally very low salinity, must be derived only after adequate scientific data are available for the particular ecosystem. Site specific evaluations using biological indicators may be necessary in these cases, especially where the natural variability is small.

Potential Sources

Salinity levels fluctuate with the penetration of tidal flows and with mixing of fresh water and marine water by wind and currents. Decreased freshwater inflows, due to the diversion of rivers and streams into impoundments such as weirs or wetlands, lead to the dissipation of salinity gradients and extended periods of elevated salinity in natural wetlands adjacent to the Broadwater. Conversely large incursions of stormwater runoff can severely depress normal salinity levels in inshore areas (ANZECC, 2000). The salinity levels of the existing wetlands is controlled by the existing amount of freshwater runoff from rain events from the upstream catchments and the tidal flushing from Trutes Bay which is limited by existing flood gates.

Management Practices

The most effective option to help alleviate the adverse effects of salinity is to minimise disruption to the natural flow regime of the water system (DNRE et al, 1998). Some specific management options are:

- minimise stormwater runoff and increase of water reuse within the development;
- minimise use of weirs and dams that will prevent natural flow through the system;
- investigate the impacts that wetlands have on the flow regime;
- awareness of upstream and downstream engineering works that could affect salinity; and
- conduct site specific evaluations using biological indicators and develop rigorous experimental modelling to create trigger values for normal ecosystem salinity.

Temperature

Aquatic ecosystem functioning is very closely regulated by temperature. Biota, and physical and chemical processes like oxygen solubility and hydrophobic interactions are sensitive to temperature changes (ANZECC, 2000). Water temperature regulates ecosystem functioning both directly through physiological effects on organisms, and indirectly, as a consequence of habitat loss.

Impact

Unnatural changes in water temperature impact indirectly upon biota through loss of supporting habitat, by changing the solubility of oxygen and calcium carbonate in water, or by influencing the extent to which metal contaminants and other toxicants are assimilated by physiological processes. Temperature is probably the most important factor influencing viral persistence in estuarine environments (AGGA et al, 2003). Water temperature influences the density, conductivity, pH, partial pressure of Carbon Dioxide and the saturation states of minerals of seawater. Water temperature also impacts the conversion of dissolved oxygen measurements to % saturation values.

Potential Sources

The main causes for water temperature change in the Tweed Area E development will be changes in the amount of freshwater flow and the extent of to which freshwater is mixed with marine water by winds and tides. There should be no major discharge sources of either hot or cooling water from municipal or industrial effluent in the Tweed Area E.

Management Practices

Temperature changes are very strongly mediated by hydraulic mixing, e.g. river flow, tidal mixing or wind-driven mixing in lakes and waterbodies (ANZECC, 2000). A well mixed waterbody will not stratify and will be buffered to some extent from the effects of thermal pollution. The two main management options to prevent thermal stratification are artificial aeration and managing water diversions such that streams and gullies continue to flow.

Artificial aeration is not expected to be required for the Tweed Area E residential development. Managing water diversions to maintain natural flow regimes as shown above (salinity) is recommended to help achieve a stable temperature distribution.

pH

pH is a measure of the acidity or alkalinity of water on a log scale from 0 (extremely acidic) through 7 (neutral) to 14 (extremely alkaline). The NSW EPA interim guidelines for pH are 5-9. The expected pollutant concentration for Tweed Area E is 6.8 (NSW EPA, 2003). The pH of the water bodies within the area and runoff generated from the catchment is not expected to cause significant problems to the environmental values of the area. A monitoring program that includes measurements of pH will determine if levels stay within guideline values.

Oil and Grease (including petrochemicals)

Oil and grease is a composite of possibly thousands of organic chemicals with different properties and toxicities (Duncan, 1999), as components of liquid and gaseous fuels, petroleum hydrocarbons are amongst the most widely processed and distributed chemical products in the world (ANZECC, 2000).

Impacts

The presence of oil and petrochemicals makes water aesthetically unattractive. They can form deposits on shorelines, and bottom sediments that are detectable by sight and odour. Some organic compounds can be absorbed directly from the water through the skin, making these substances even more undesirable in recreational areas (ANZECC, 2000).

The lighter oil fractions (kerosene, petrol, benzene, toluene and xylene) are much more toxic to fish than the heavy fractions (heavy paraffins and tars). Fish species can differ significantly in their sensitivity to these compounds.

In general, oils of animal or vegetable origin are chemically non-toxic to aquatic life, although they can taint the flesh of food species, coat gills reducing oxygen uptake, increase BOD levels and increase maintenance of water treatment equipment.

Potential Sources

Primary sources in surface waters include runoff from roads, car parking areas and discharges from areas using oil. Sources of oil and grease include food processing and preparation, operation and maintenance of vehicles and machinery, and natural compounds leached from vegetation and plant litter.

Management Practices

Useful structural stormwater treatment measures for oil and grease are given below:

- oil and grit separators;
- sand filters;
- infiltration trench/basin;
- porous pavements; and
- constructed wetlands.

These appropriate treatment measures are able to help mitigate oil and grease in the water system. The optimum treatment methods from those available are sand filters and constructed wetlands.

Preventing the pollutant at the source is a positive option to assist in reaching guideline oil and grease values. Source management options include:

- encouragement and education of responsible resident disposals — all oil from the house disposed of correctly;
- minimise food disposals from restaurants and food industries in the residential area; and
- providing car parking areas with suitable oil collection systems such as oil and grit separators.

Appendix F shows the pollutant reduction efficiencies for the oil and grease management practices.

Litter

Litter includes paper, plastic, glass, metal and other packaging materials.

Impacts

The impacts of litter are primarily aesthetic, but also pose a risk to aquatic ecosystems by preventing plant growth and entrapping animals. Litter may not indicate the degree to which the water is affected by chemicals, nutrients and bacteria but is often seen by the community as a sign of poor water quality. The poor visual appearance of the water system can perpetuate a depressing image, reduce the environmental and recreational facility of the river and set a poor example for people and actually encourage more littering (AGGA, 2003).

Potential Sources

Litter is generally associated with human activities that result in waste generation. Litter can be deposited in the catchment in a number of ways such as deliberate pollution or overflows from rubbish bins. Once litter is on the ground it can easily be transported by storm runoff into stormwater systems and washed into local gullies and creeks.

Management Practices

Useful structural stormwater treatment measures for litter are given below:

- in ground gross pollutant traps (GPTs);
- open GPTs;
- water quality ponds;
- filter strips;
- litter and trash racks;
- litter booms;
- downwardly inclined screens; and
- constructed wetlands.

These appropriate treatment measures are able to help mitigate litter problems in the water system. The optimum treatment methods from those available are in-ground GPTs, open GPTs water quality ponds and constructed wetlands (BCC, 2000).

Managing litter generation at the source is a major beneficial option to assist in preventing litter problems. Source management options include:

- Installation of rubbish bins throughout the Tweed Area E development area, particularly recreational areas such as parks and shops.
- Street sweeping – is a widely used practice to reduce the amount of street borne pollutants entering the stormwater system (DNRE et al, 1998). Coordination and integration between street cleaning and other maintenance activities is essential to maximise the benefits of street cleaning.
- Encouragement and education of responsible resident disposals — all litter from the residential area should be disposed of correctly.

Appendix F shows the pollutant reduction efficiencies for the litter management practices.

Chemical Contaminants

Chemical contaminants may be categorised into three broad groups (ANZECC, 2000).

- ***Inorganic chemicals (mostly heavy metals):*** These are a potential problem for human health, particularly in the case of bivalve molluscs where bioaccumulation increases the concentrations of toxicants. The rate of accumulation is species specific and depends on the mechanism of absorption and tissue distribution.
- ***Organic chemicals (pesticides and herbicides):*** This broad group includes synthetic compounds which through either bioaccumulation or residue concentrations are potentially toxic to human consumers of contaminated aquatic foods.
- ***Radionuclides (radioactive elements):*** Any man-made or natural element that emits radiation and that may cause cancer after many years of exposure through drinking water.

Impacts

Waters containing chemicals that are either toxic or irritating to the skin or mucous membranes are unsuitable for recreation. In general, there are two kinds of human exposure in swimming areas: contact with the waterbody and ingestion of the water. Many pesticides are broken down into harmless products by microorganisms.

Potential Sources

Heavy metals in the residential area will mainly be sourced from roads, roofs, cars and paints. These will usually enter waterways via runoff. Pesticides and fertilisers enter water from land by aerial drift, runoff or leaching into groundwater.

Management Practices

Useful structural stormwater treatment measures for chemical contaminants are given below:

- constructed wetlands;
- grass swales;
- sand filters;
- infiltration trench/basin; and
- porous pavements.

These appropriate treatment measures are able to help mitigate chemical contamination problems in the water system. The optimum treatment methods from those available are constructed wetlands, infiltration trenches and basins and porous pavement (BCC, 2000).

Managing chemical contaminant problems at the source will limit the risk of exceeding desired water quality objectives. Source management options include:

- reduction of use of fertilisers around the residential areas; and
- integrated pest management practices minimise pesticide usage by careful monitoring of pest species (and their predators) and utilising a range of pest control options.

Appendix F shows the pollutant reduction efficiencies for the heavy metals management practices.

3.4.3.12 Environmental flows

The NSW Government has developed interim water quality objectives through the Environment Protection Authority to ensure the long-term health of all waterways. Interim river flow objectives have been established to provide measurable objectives to protect environmental values including aquatic ecosystems. The river flow objectives (RFOs) are provided to maintain or improve river health by altering flow patterns to a more natural flow regime. The RFOs applicable to the Tweed River are presented below:

- mimic natural drying in temporary waterways;
- maintain natural flow variability;
- maintain natural rates of change in water levels;
- manage groundwater for ecosystems;
- minimise effects of weirs and other structures;
- maintain wetland and floodplain inundation; and
- maintain or rehabilitate estuarine processes and habitats.

Development of the Tweed Area "E" catchment will change the level of imperviousness and increase flow volumes, frequencies and peak discharges. Measures will be required to meet the interim RFOs discussed above. The adopted WSUD strategies will limit the impact of development, however it is not possible to mimic these flow patterns completely as the adopted wetlands will require sufficient water to sustain wetland plants throughout extended periods of dry weather.

A MUSIC model was established using 27 years of daily rainfall for 1967 to 1995. 1982, 1993, and 1994 data were removed from the data set due to incomplete records. The maximum rainfall occurred in 1967 with 2969 mm, the lowest in 1986 with 793 mm, and the average rainfall for the period was 1720 mm. A natural catchment model was established and a cumulative frequency plot produced of daily flow volumes entering the Terranora Broadwater. A developed and unmitigated catchment model was also produced and run for the same 27 year period. The results of both model runs are plotted below as Figure 3.12.

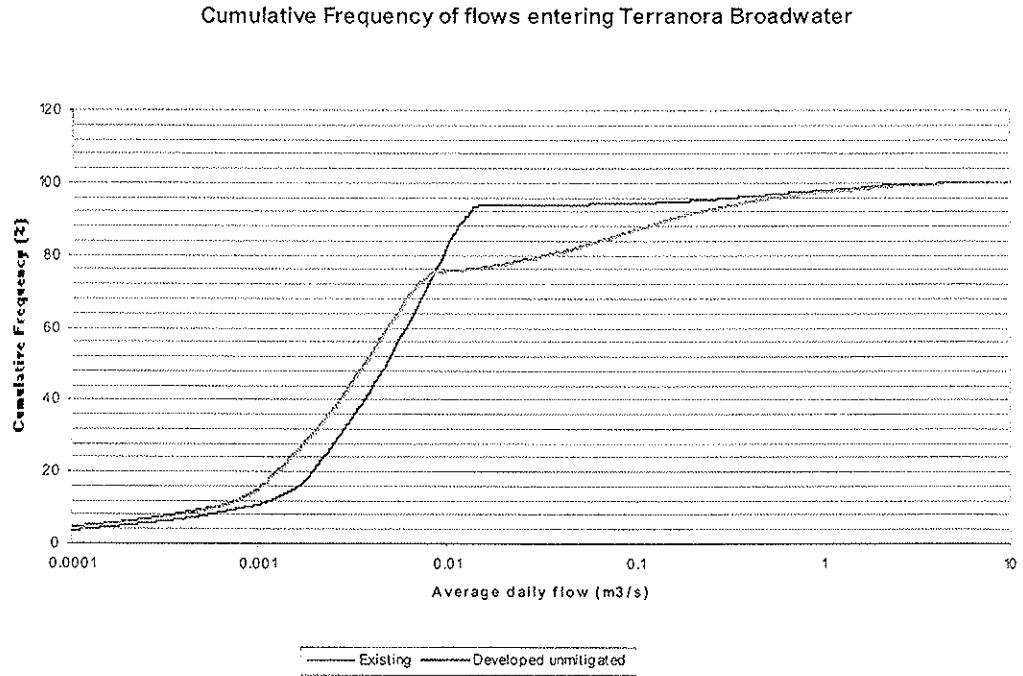


Figure 3-12: Development impact on daily flow frequency

Figure 3.12 shows that the developed unmitigated catchment has a lower cumulative frequency of average daily flows between 0.008 m³/s and 0.6 m³/s, or alternatively a higher frequency or occurrence of these or larger flows. This is expected due to the increase in impervious areas due to development. The maximum increases in frequency were flows in the range 0.01 to 0.02 m³/s.

The impact of this increase is difficult to assess without undertaking a long term water balance of inflows into the natural wetlands to determine the influence this would have on the natural wetland inundation and drying regime. However an assessment of the cumulative frequency will provide an estimation of the relative recurrence intervals of the flows that are impacted most by development. The cumulative frequency for a range of flow durations, based on the 27 year MUSIC model, is provided below in Table 3.28.

Table 3-28: Cumulative frequency statistics

Event	Number of occurrences in 27 years	Daily Chance of occurrence (%)	Cumulative Frequency (%)
Q 1 month	324	3.3	96.7
Q 2 month	162	1.6	98.4
Q 3 month	108	1.1	98.9
Q 4 month	81	0.82	99.2
Q 6 month	54	0.55	99.4
Q 9 month	36	0.37	99.6
Q 1 year	27	0.27	99.7

Using the information in the previous table, a flow that would on average be expected 12 times a year (Q 1 month) from the developed catchment would equate to an average daily flow of around 0.80 m³/s. This is an increase of around 45% from the average daily flow of 0.55 m³/s from the natural catchment. This is highlighted below in Figure 3.21.

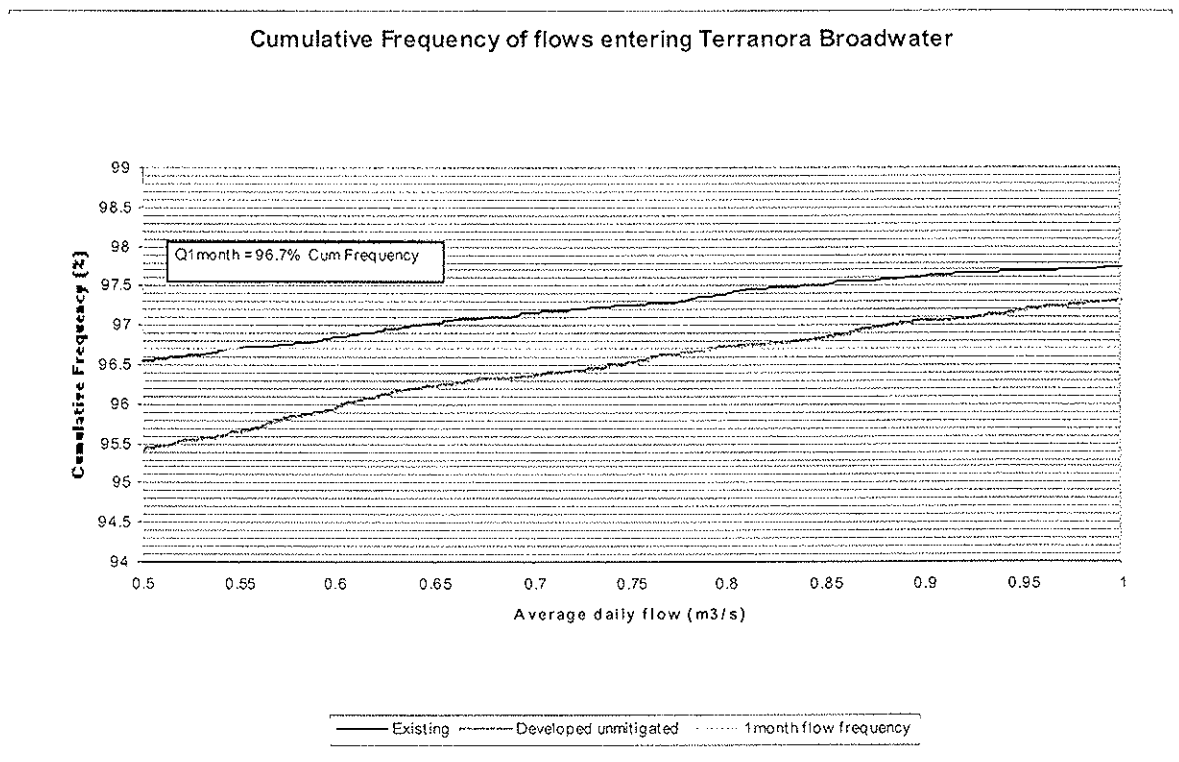


Figure 3-13: Development impact on Q 1 month flows

The impact of development on the less frequent flows (i.e. an average recurrence interval of greater than one month) is less as the cumulative frequencies approach each other. The results indicate that the Q3 month flow changes from 1.9 m³/s to 2.1 m³/s (11% increase) and the Q6 month flow changes from 2.9 m³/s to 3.1 m³/s (7% increase).

The impact of the treatment train mitigation measures was observed through the development of a separate model that included grass swales, bio-retention, rainwater tanks, and wetlands. The model results are provided as a cumulative frequency plot as shown in Figure 3.14.

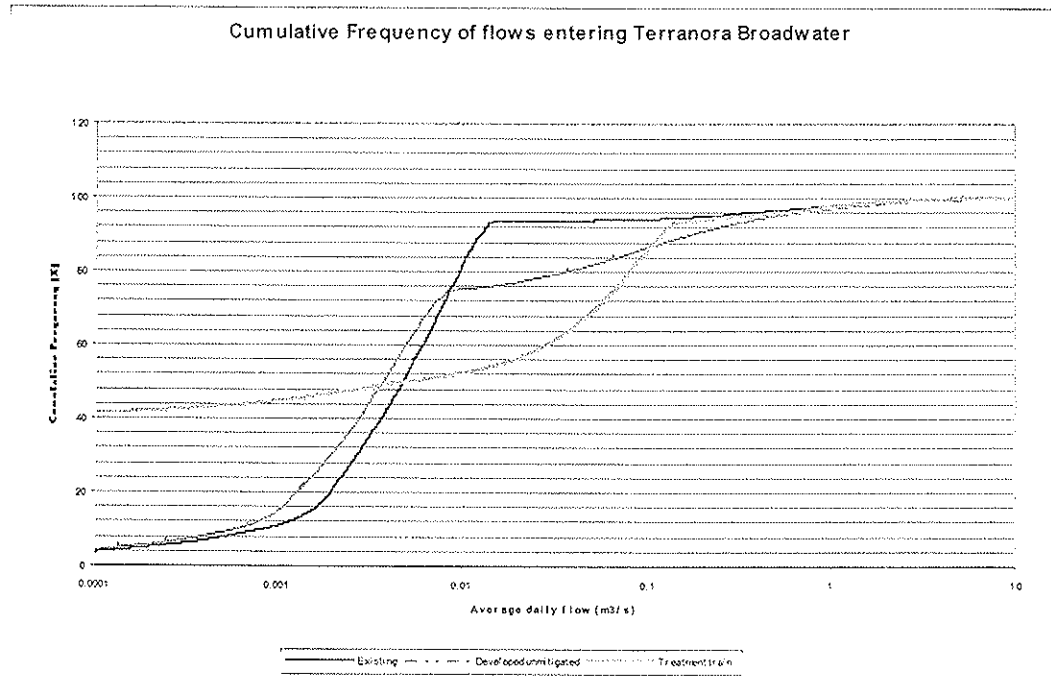


Figure 3-14: Treatment train impact on daily frequency

The treatment train results indicate that the development impacts were mitigated by the wetlands with similar frequencies for average daily flows in the range of 0.1 m³/s to 10 m³/s. This equates to a cumulative frequency of 85% or a flow (surface flow and base flow) which would be expected to occur approximately 55 times on average per year. The results then indicate that the system produces a higher frequency of flows between 0.01 m³/s and 0.1 m³/s. This is due to the outlet configuration which promotes a nominal residence time of 72 hours within the wetland. The wetland will temporarily store water for this period and then release the extended pool volume. This equates to an increased lower flow discharge over a number of days, increasing the frequency of these low flow events. In summary, the treatment train approach will mimic the natural flows better than the developed unmitigated case for flows with a frequency less than the Q 1 month.

The modelling also shows that the extremely low flows (average daily flow rate of 0.003 m³/s) are completely retained by the wetland and prevented from entering the Terranora Broadwater. This can be overcome by allowing a low flow bypass to allow flow to continue past the wetland and enter the Broadwater directly. This flow will not be treated (apart from the removal of gross pollutants through a GPT) and will lower the effectiveness of the wetland, however it will better mimic the lower frequency small natural flows. Alternatively, a small discharge pipe could be provided in the wetland to discharge low flows from the wetland from the permanent store. Long term daily water balancing modelling would be required to ensure that sufficient water is retained to maintain the health of wetland plants.

A model run was completed with a small discharge pipe that allows for an environmental flow of 1L/s (modelled as a low flow bypass in MUSIC) from the wetlands. This equates to around 86 m³ per day which would fully drain Wetland 1 in around 100 days neglecting the impact of evaporation and additional rainfall. Similarly Wetland 2 and 3 would drain in around 400 and 175 days respectively, indicating that it may be possible to allow for small environmental flows without compromising the health of wetland plants. Figure 3.15 shows the MUSIC model results that indicate if small environmental flows are allowed to bypass or be discharged from the wetland, that the flow frequency would approach the natural flow regime.

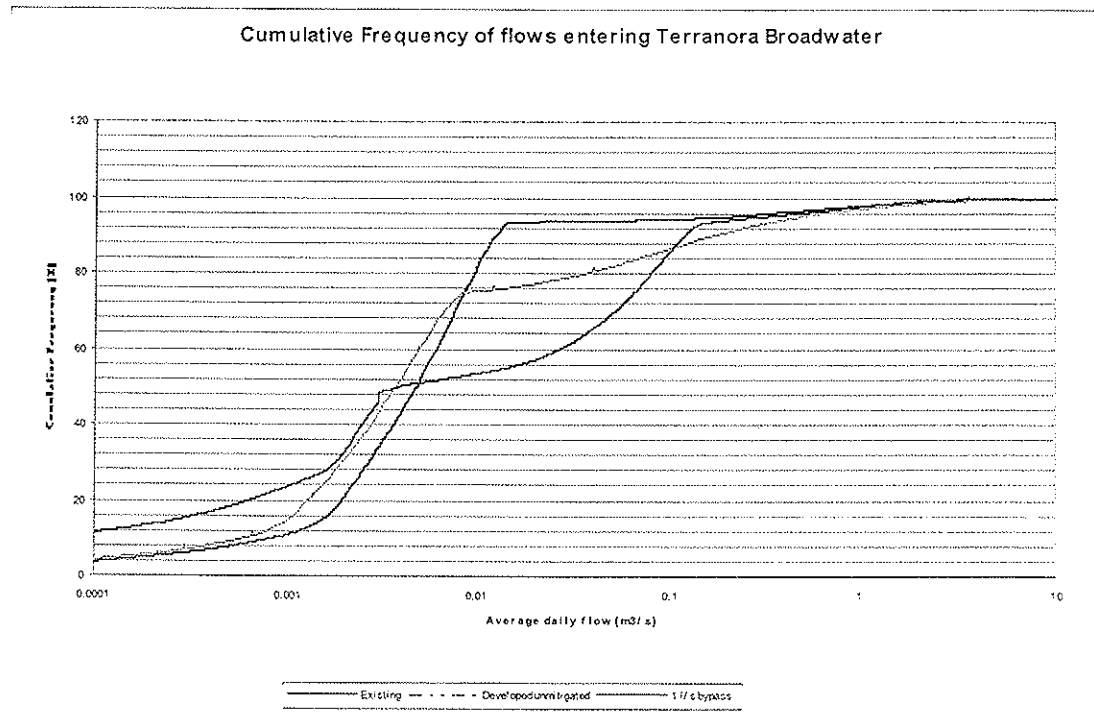
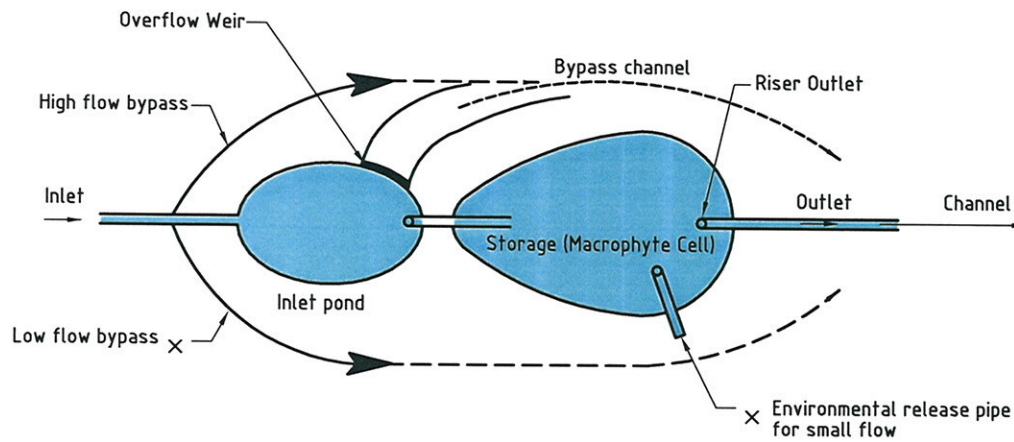


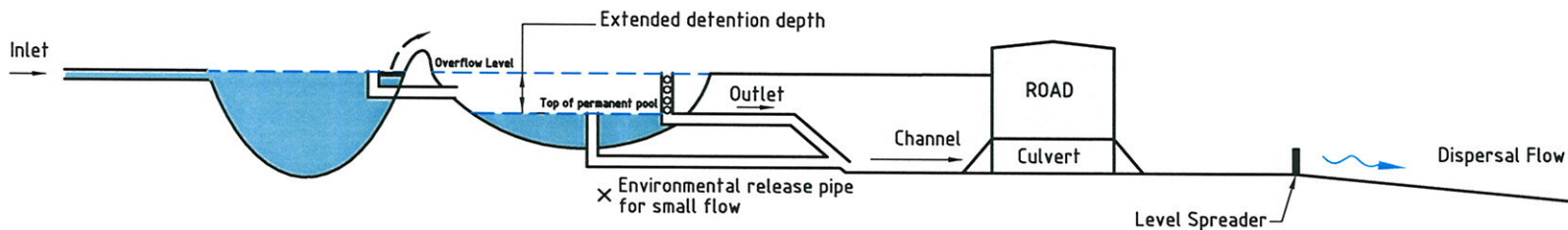
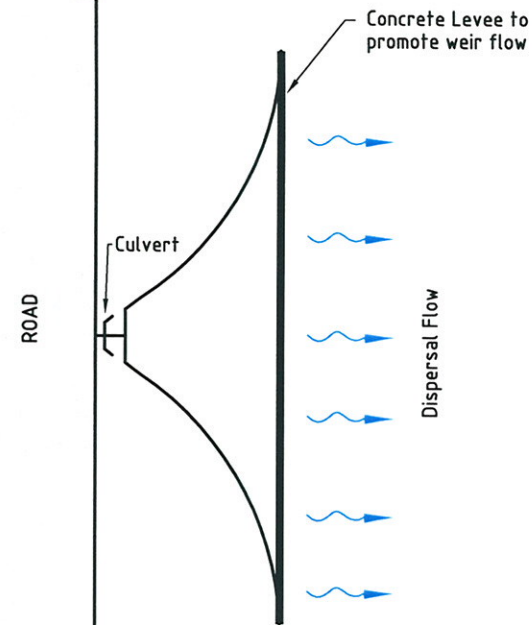
Figure 3-15: Environmental bypass cumulative frequency plot

It is suggested that the low flow environmental pipe option be adopted for any wetlands within the Tweed Area E to better mimic natural flows. A long term water balance would be required to confirm that the wetlands do not drain and impact the health of wetland plants.

A conceptual layout for the wetlands is provided below.



PLAN VIEW



LONGITUDINAL VIEW

NOTES

A detailed water balance can determine what allowable flow rate should be provided for small environment flows.

- × Only one of the flow paths (low flow bypass or the environmental release pipe) is required

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	Project TERRANORA AREA 'E' CONCEPTUAL WETLAND LAYOUT	Drawing No FIGURE 3-16
	Cad File FIG-3.21.dwg	Rev 1

The recommended treatment train approach, with an environmental low flow pipe, provides the best fit with natural flows into the Terranora Broadwater and assists in meeting the RFOs. Matching natural average daily flow frequencies will:

- assist in attaining natural creek and gully drying periods;
- mimic natural flow variability for frequent and infrequent flow events;
- assist in attaining natural rates of change in water levels; and
- mimic natural patterns of wetland inundation.

A level spreader is also proposed at the inlet to the existing wetlands adjacent to the Broadwater. The purpose of the level spreader is to distribute flows across a much wider area than would be expected from a normal inlet channel. This is expected to prevent concentrated flows with high velocities entering and scouring the wetlands, and provide a more natural flow path.

3.4.4 Water quantity

Development has the potential to lead to significant changes in catchment hydrology due to a change in the pervious/impervious areas on site, in the storage capacity of the site and the concentration of flow paths. Without management, the increase in peak stormwater flows could lead to flows with higher velocities that could erode and scour of gullies, damage riparian vegetation, in addition to increased flood levels.

An XP-RAFTS model was developed to determine peak stormwater flows from the catchments. Three scenarios of stormwater quantity were investigated for Terranora Area 'E'.

- Original – the quantity of stormwater produced from the Terranora Area 'E' catchment prior to any rural or urban development, was determined to obtain an indication of the quantity of stormwater that would have flown into wetlands thought to be freshwater at this time.
- Developed – the quantity of stormwater expected to be produced when Terranora Area 'E' has been totally urban developed.
- Developed with mitigation – the quantity of stormwater produced from the totally urban developed Terranora Area 'E' catchment with detention basins added to return stormwater flows to their original levels.

This section discusses the modelling undertaken, results and required mitigation.

3.4.4.1 XP-RAFTS model setup

XP-RAFTS is a non-linear routing program which develops stormwater runoff hydrographs for design storms using Intensity-Frequency-Duration data and Australian Rainfall and Runoff (AR&R) storm temporal patterns. The initial/continuing loss model was used to generate excess rainfall, and the reservoir (pond) routing model was used to allow routing of inflow hydrographs through retention basins.

The catchment and sub-catchment areas and flow paths modelled in XP-RAFTS were determined using an electronic version of McLauchlan Surveying Property Boundaries, Detail & Contours for Area 'E' Terranora drawing and MFA Consulting Engineers Figure 9 from Appendix D of the Jim Glazebrook & Associates Pty Ltd "Area E" – Terranora – Planning Report & Structure Plan for Terranora Landowners Group, October 2002.

To determine the percentages of pervious and impervious land, each sub-catchment was divided into land use categories (rural, rural residential, commercial, urban and open space) for the original and developed scenarios. The original scenario was assumed to be 100 % open space and the developed scenario was based on figures provided in the "Area E" – Terranora – Planning Report & Structure Plan (Glazebrook & Associates 2002). The percentage impervious for each land use category was obtained from the Queensland Urban Drainage Manual (QUDM) and are tabulated below.

Table 3-29: Percentage impervious for land use categories

Land use category	Percentage impervious
Rural	10 %
Rural Residential	20 %
Commercial	90 %
Urban	35 %
Open Space	0 %

The Manning's n for the impervious fraction of the sub-catchment is 0.015 from QUDM. The Manning's n for the pervious fraction of each land use category was obtained from QUDM as tabulated below.

Table 3-30: Pervious Manning's n

Land use category	Manning's n
Rural	0.07
Rural Residential	0.05
Commercial	0.025
Urban Pervious	0.025
Open Space	0.1

Initial loss for pervious catchments was assumed as 20 mm and continuing loss was assumed as 2.5 mm/hour based on AR&R recommendations for east of the western slopes in New South Wales. Initial loss for impervious catchments was assumed as 1.5 mm and 0.0 mm/hour for continuing loss based on XP-RAFTS manual recommendations.

Typical cross-sections and slopes were entered for each channel modelled, based on existing topography, determined using an electronic version of McLauchlan Surveying Property Boundaries, Detail & Contours for Area 'E' Terranora drawing.

For the developed case, the existing farm dams were considered to be full and therefore only the storage capacities above full supply level were considered. These were determined using an electronic version of McLauchlan Surveying Property Boundaries, Detail & Contours for Area 'E' Terranora drawing.

Figure 3.17, 3.18 and 3.19 below show the layout of the original model and the developed models. Circles are nodes to which catchments and/or basins can be attached and the thick lines indicate where channels have been modelled. Junction 1, 2 and 3 were used to determine the quantity of flow reaching the wetlands. The adopted sub-catchment layout matches the MUSIC layout discussed in Section 3.3.

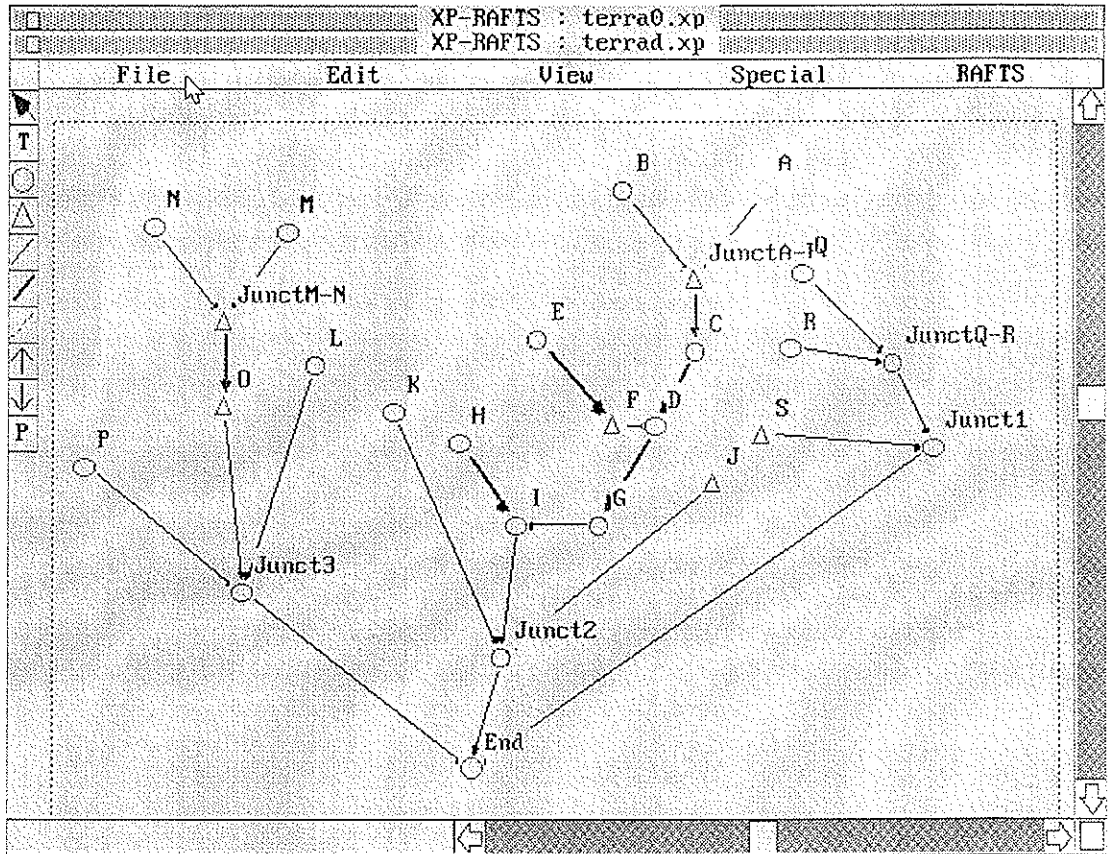


Figure 3-17: Original model layout

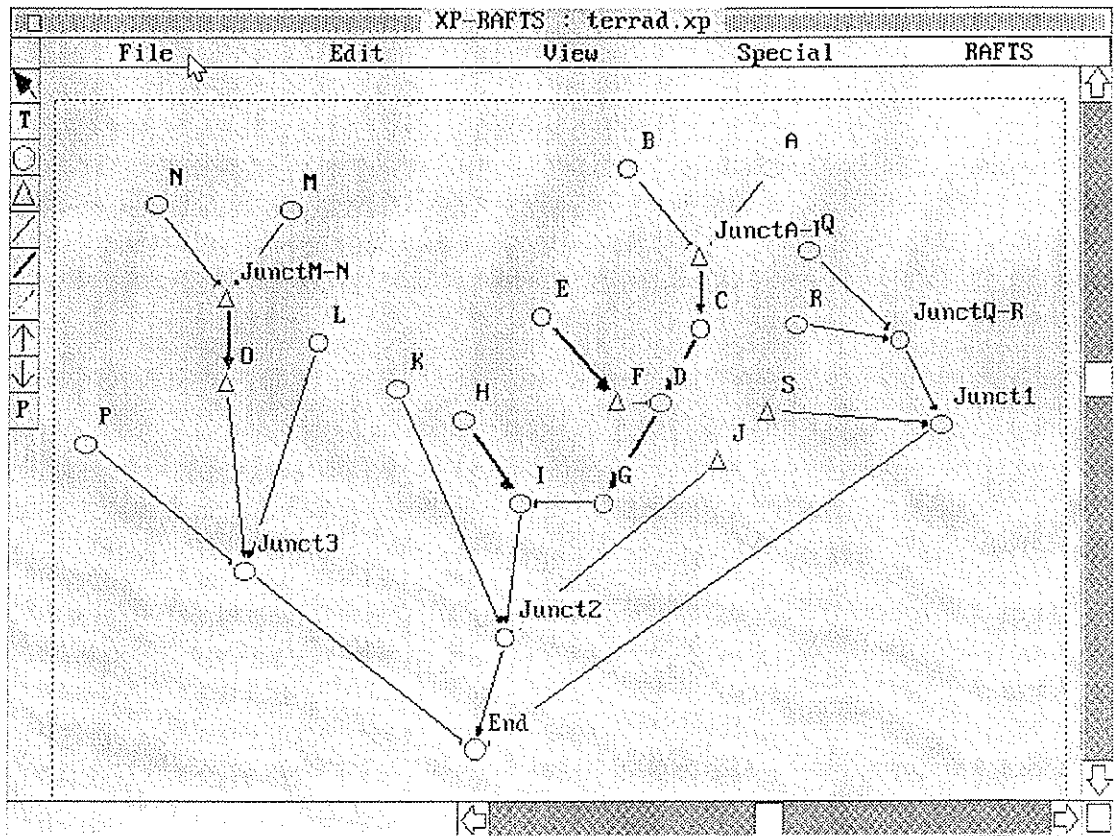


Figure 3-18: Developed model layout

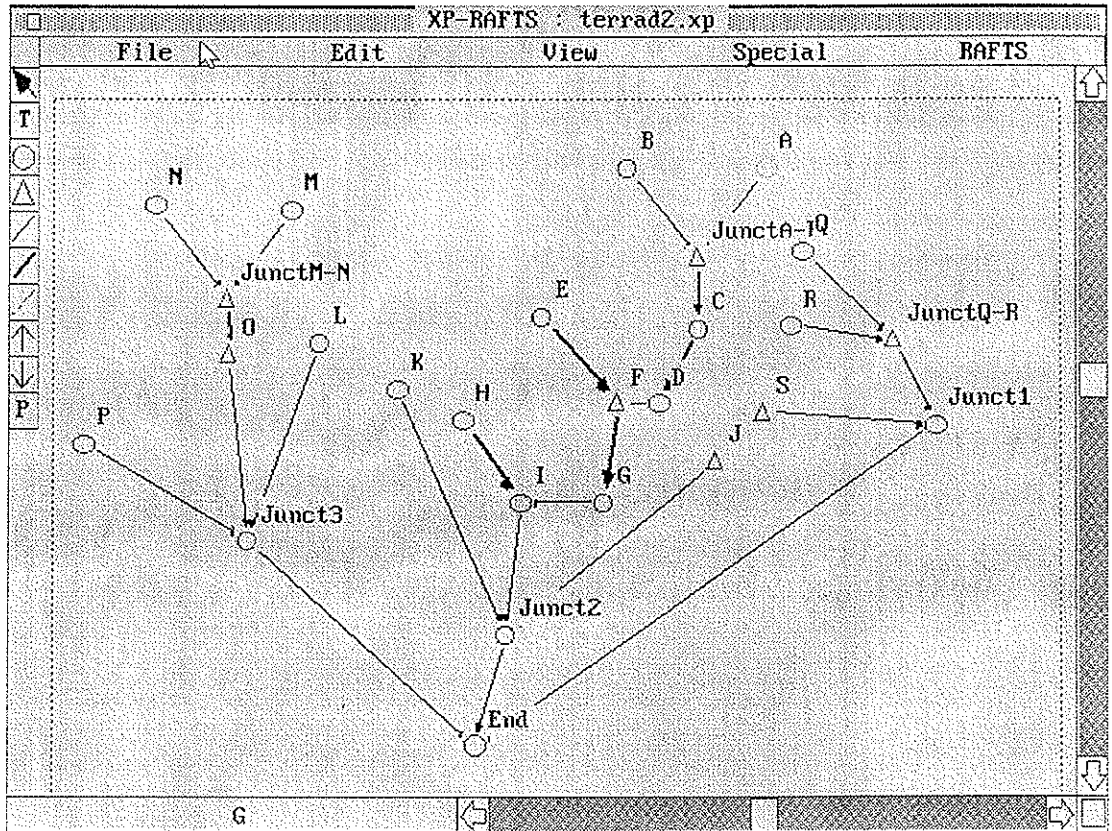


Figure 3-19: Developed with mitigation model layout

3.4.4.2 Results

3.4.4.2.1 Peak storm

The 10 minute, 20 minute, 30 minute, 1 hour, 2 hour, 3 hour, 6 hour, 12 hour, 24 hour and 48 hour, 100 year Average Recurrence Interval (ARI) storms were run in XP-RAFTS to determine the critical storm duration for the catchment. The peak flow for each storm duration for the major junctions entering the wetlands are shown in the figures below.

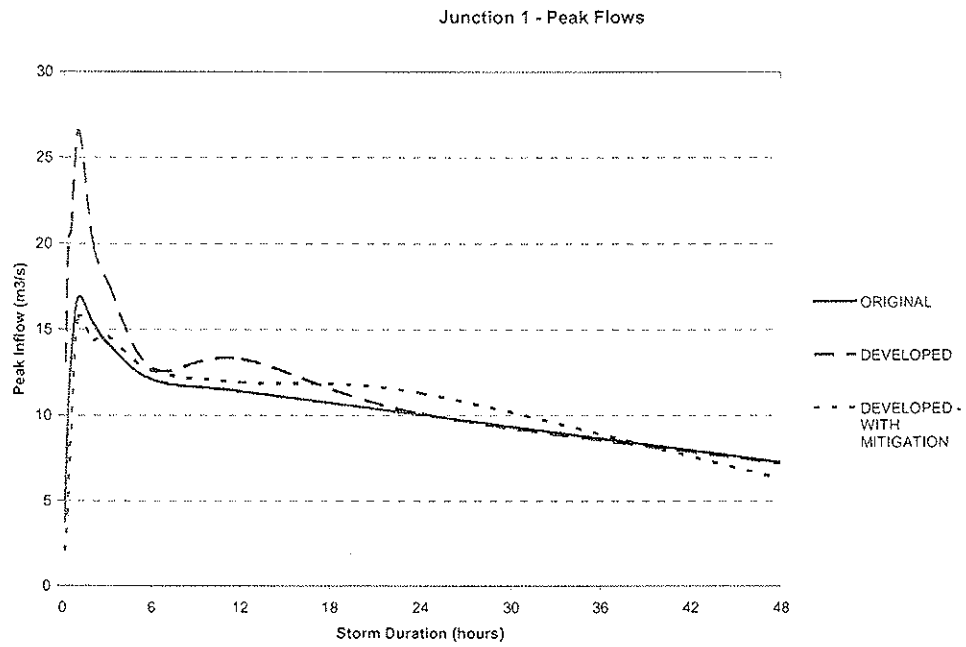


Figure 3-20: Junction 1 – peak flows

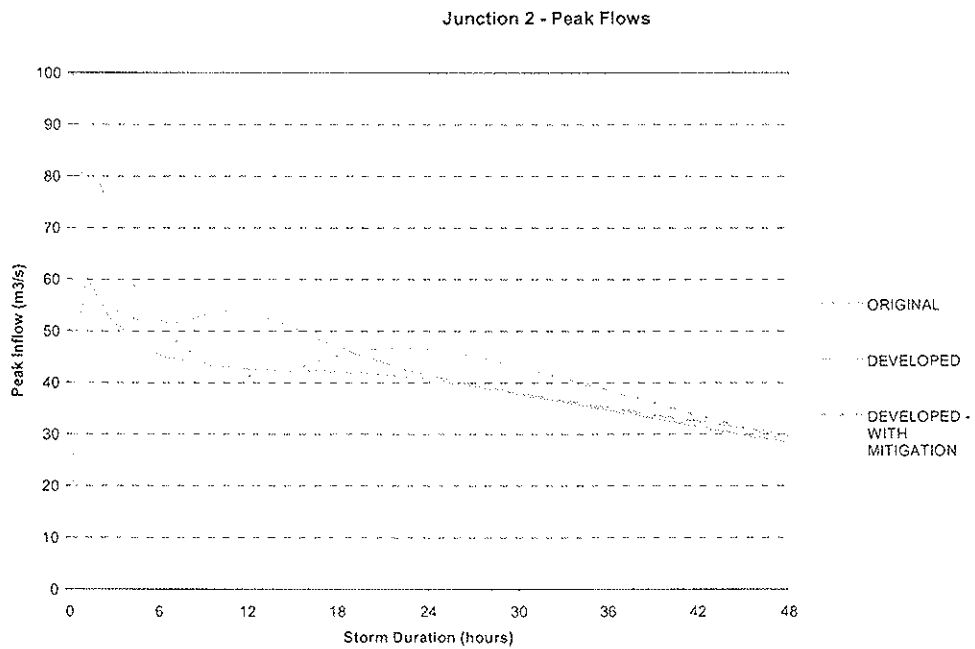


Figure 3-21: Junction 2 – peak flows

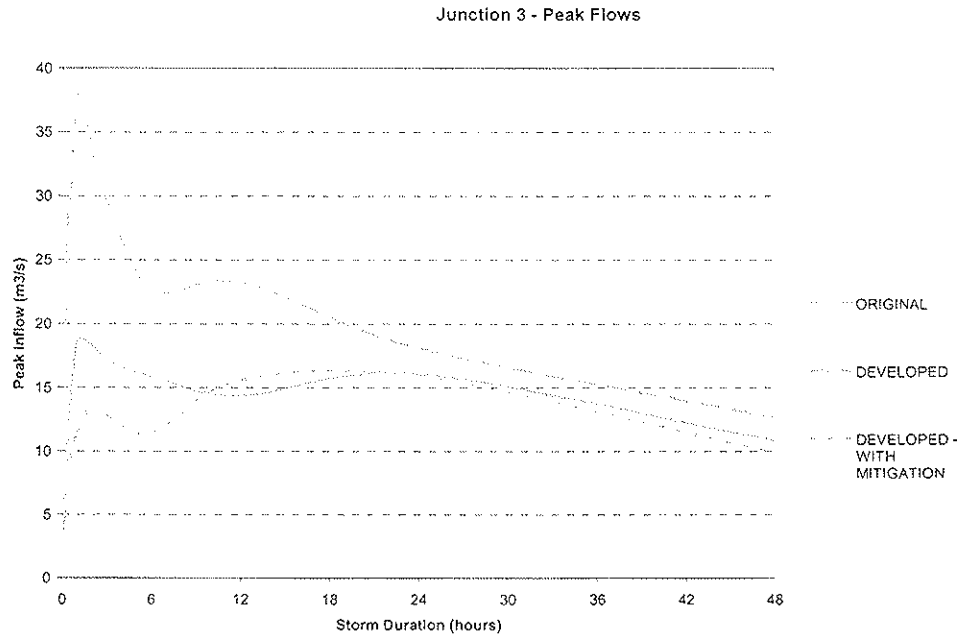


Figure 3-22: Junction 3 – peak flows

The peak for Junction 1 and 2 is the 1 hour storm for the original, developed and developed with mitigation scenarios. For Junction 3 the peak storm is 1 hour for the original and developed scenarios, and moves to the 24 hour storm for the developed with mitigation scenario.

3.4.4.2.2 Peak storm hydrographs

The hydrographs for the peak storm for developed and original scenarios are plotted below.

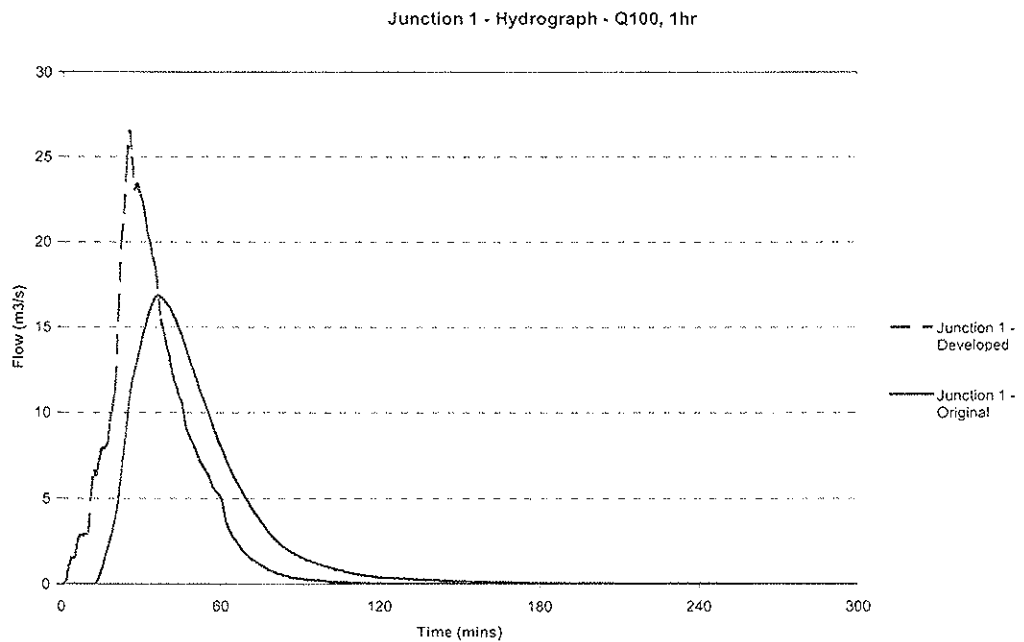


Figure 3-23: Junction 1 hydrograph

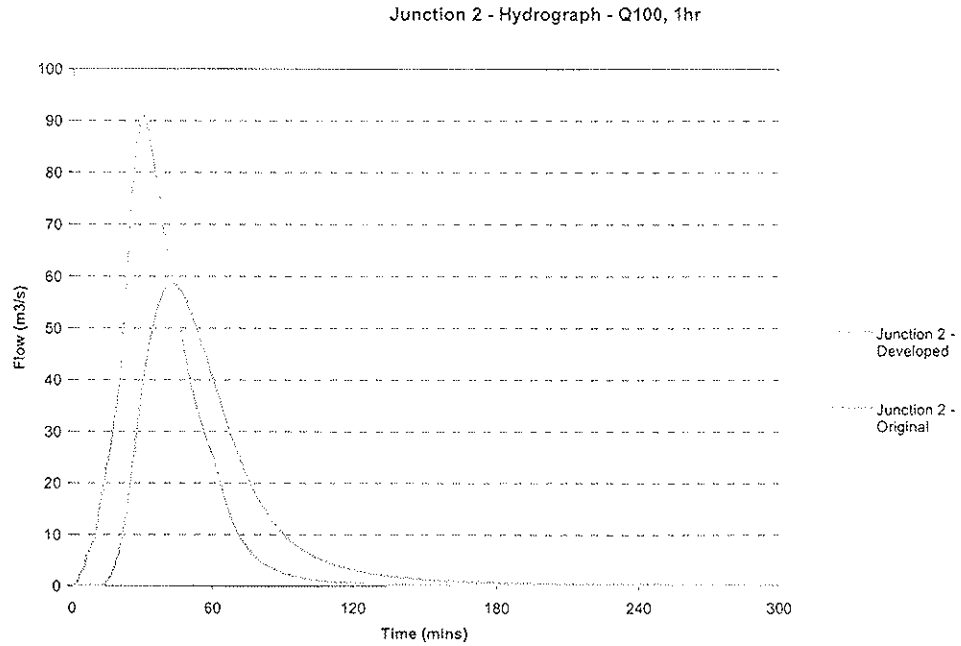


Figure 3-24: Junction 2 Hydrograph

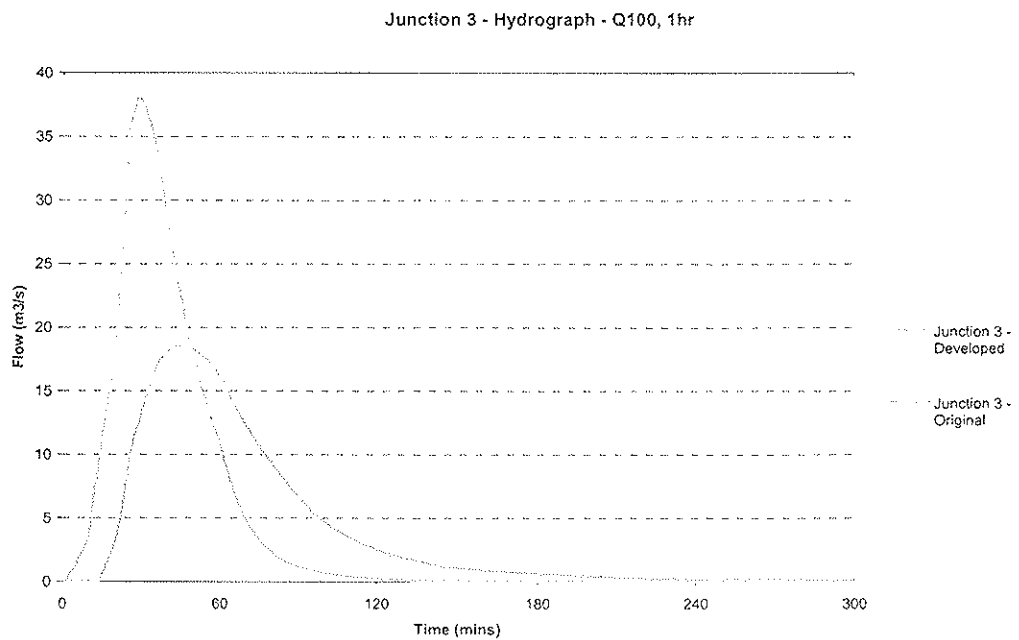


Figure 3-25: Junction 3 hydrograph

These hydrographs demonstrate the change in peak flow volume between the original and developed scenarios.

To reduce the increase in peak runoff due to urbanisation, (the difference between the two curves), mitigation in the form of detention basins can be added.

For the Developed with Mitigation scenario, the following table illustrates the detention basins required to mitigate the peak storm developed flows to original levels.

Table 3-31: Detention basin details

Basin Node Location	Maximum Storage (m ³ /s) ¹	Depth of Storage below spillway (m)	Spillway width (m)	Depth of Water over Spillway (m)	Spillway Q100 Flow (m ³ /s)
Junct Q-R	18000	3.7	20	0.5	11.2
S ²	2050	0	10	0.5	5.5
J ²	260	0	10	0.5	6.6
F	48800	3.1	30	0.8	36.0
Junct M-N ³	10350	2.7	25	0.4	8.7
O ³	43350	4.7	30	0.4	13.5

1. These are in addition to any existing farm dams.
2. Relies on existing farm dam.
3. Peak Storm is 24hr duration.

The addition of these storages produces the following hydrographs.

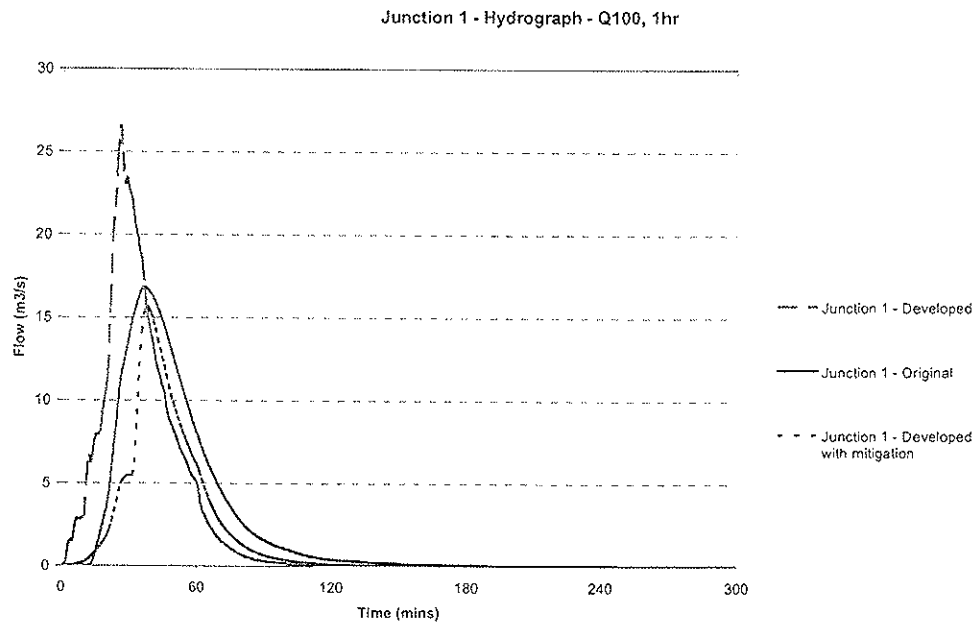


Figure 3-26: Junction 1 hydrograph

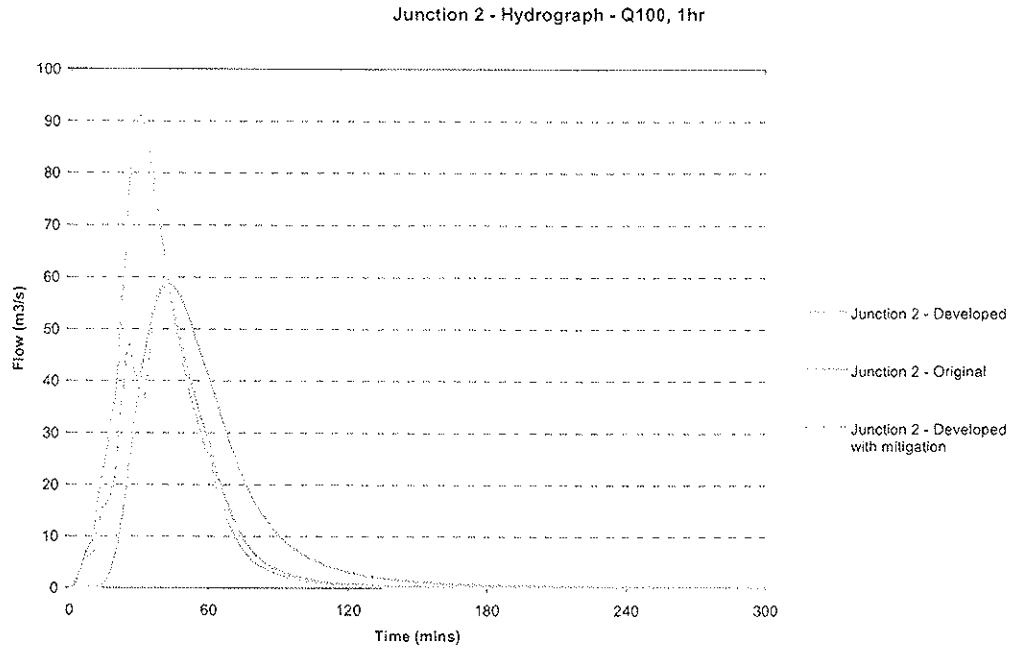


Figure 3-27: Junction 2 hydrograph

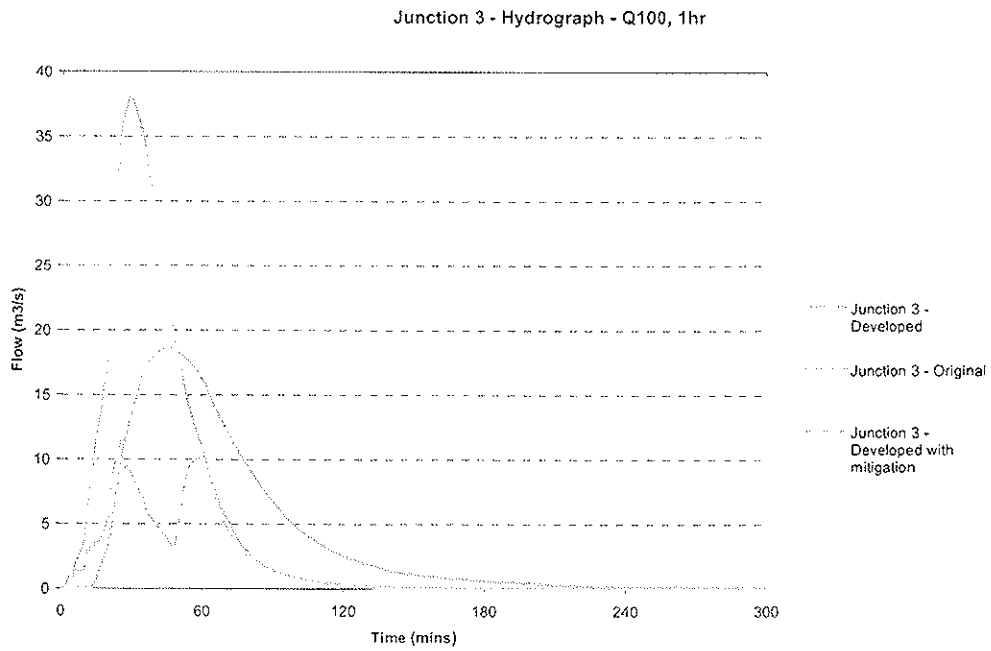


Figure 3-28: Junction 3 hydrograph (1 hour storm duration)

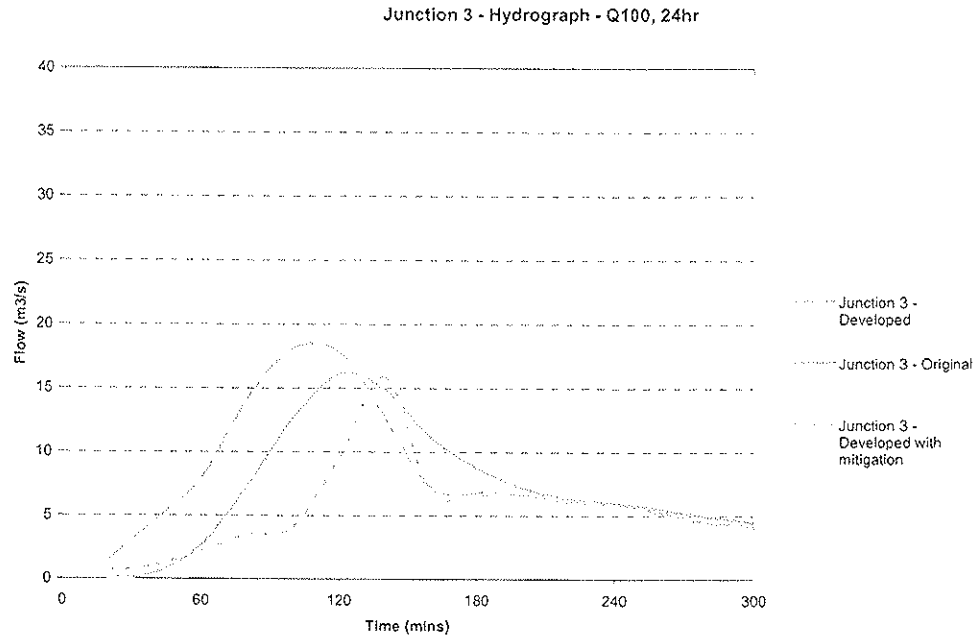


Figure 3-29: Junction 3 hydrograph (24 hour storm duration)

In all cases the peak of the developed with mitigation flows are equal to or less than the predicted original flows for this design storm.

The twin peaks produced on the developed with mitigation hydrograph for Junction 2 is the result of not all flows from the catchment being attenuated in the detention basins.

The twin peaks produced on the developed with mitigation hydrograph for Junction 3 (1 hour storm duration) is the result of the detention basin at 'O' peaking prior to the detention basin at 'Junct M-N' peaking. The 24 hour storm duration has both detention basins peaking at almost the same time, making this storm duration more critical than the 1 hour storm.

The results from RAFTS models are summarised in Tables 3.32 and 3.33 below.

Table 3-32: Channel flow results – (1 hour storm duration)

Channel	Original Max Flow (m ³ /s)	Developed Unmitigated Max Flow (m ³ /s)	Developed Mitigated Max Flow (m ³ /s)
JunctA-B – C	13.6	26.2	26.2
C – D	20.4	38.8	38.8
E – F	6.4	12.5	12.5
F – G	32.9	53.3	35.7
H – I	7.7	14.3	14.3
JunctM-N - O	7.7	18.5	17.2

Table 3-33: Channel flow results – (24 hour storm duration)

Channel	Original Max Flow (m ³ /s)	Developed with Mitigation Max Flow (m ³ /s)
JunctM-N - O	7.1	9.1

The channels between JunctA-B – C, C-D, E-F, H-I are upstream of detention basins and therefore these flows are not reduced.

Channel F-G, follows the detention basin at node F and therefore the developed with mitigation flows, depth and velocity are very similar.

Channel JunctM-N – O, is between the detention basin at JunctM-N and O. In the one hour storm, the detention basin at O is mitigating most of the flows, however for the 24 hour storm, the detention basin at JunctM-N mitigates most of the flows. Therefore for the 24hour storm the original and developed with mitigation flows, depth and velocity are similar, however in the 1 hour storm they are only partially mitigated from the developed results.

3.4.5 Hydraulics

A HEC-RAS model was developed to get an appreciation of flow depths, velocities and widths along the major channels within Terranora Area 'E', using flows from the Developed (without mitigation) XP-RAFTS model and cross sections developed from the McLauchlan Surveying Property Boundaries, Detail & Contours for Area 'E' Terranora drawing.

This section discusses the modelling undertaken and results.

3.4.5.1 HEC-RAS model set-up

HEC-RAS models have been prepared to determine corridor widths required to remain undeveloped for the 1 in 100 year Average Recurrence Interval (ARI) event.

The channels flowing into Junction 2 and Junction 3 carry the majority of flow into the wetlands and were therefore modelled.

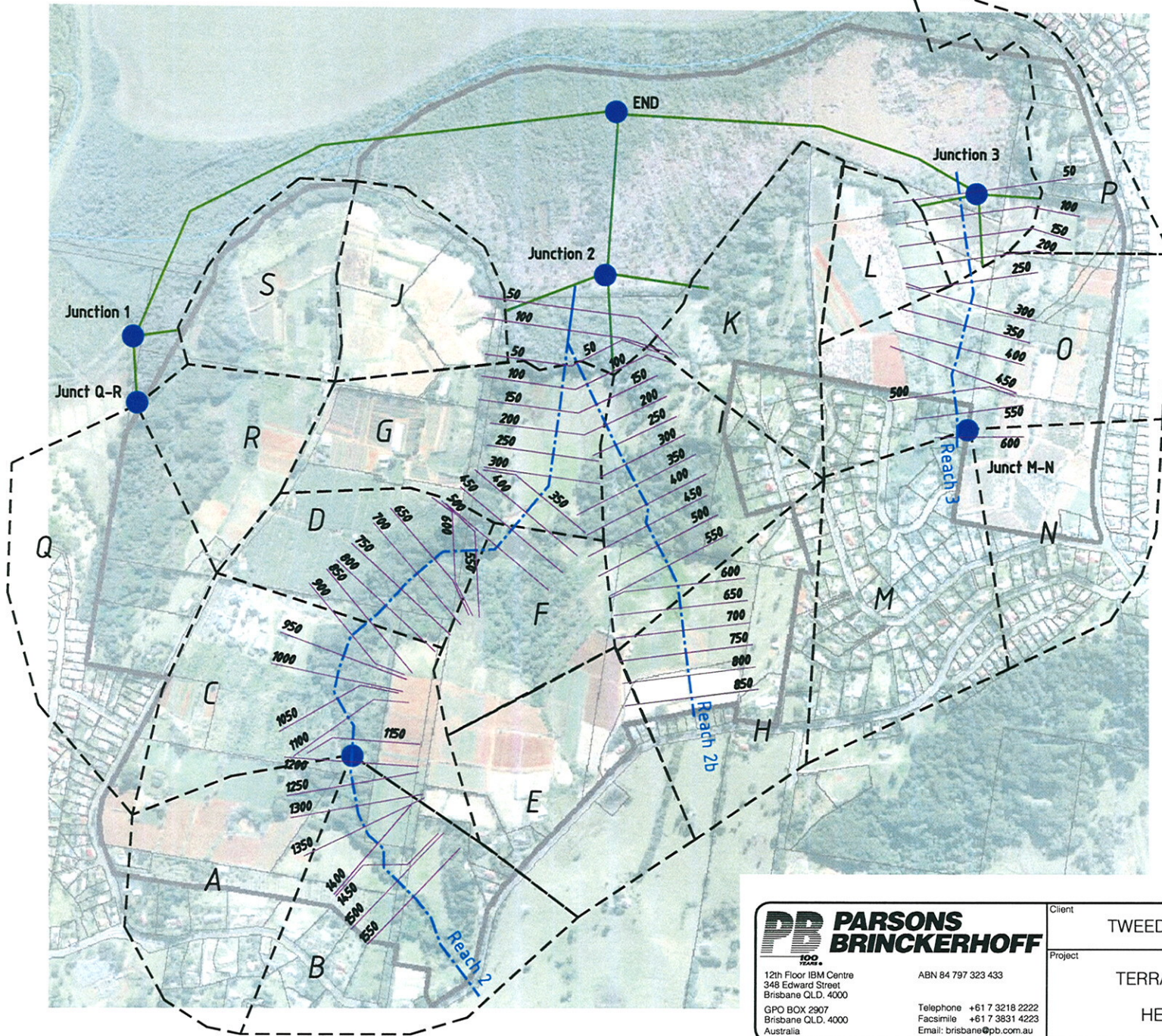
These channels were assessed using steady state HEC-RAS hydraulic models. The steady state mode of HEC-RAS is designed to calculate one dimensional flow conditions for steady gradually varied flow. Steady state assumes that flow is constant in time. User inputs to the model include channel and flood plain geometry, roughness characteristics, inflows and downstream boundary conditions.

Junction 2 and Junction 3 HEC-RAS models extend from the Terranora Area 'E' wetlands upstream to the extent of defined channel.

Topography

An electronic version of McLauchlan Surveying Property Boundaries, Detail & Contours for Area 'E' Terranora drawing, was used to determine channel extents and develop HEC-RAS cross sections.

Figure 3.30 shows the layout of the HEC-RAS models, highlighting the location of the model cross sections.



LEGEND

- Junctions
- Catchment Boundaries
- Junction Connections
- Hec-Ras Cross Sections
- River String



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	Project TERRANORA AREA 'E'		Drawing No FIGURE 3-30	
	HECRAS LAYOUT		Cad File FIG-3.35.dwg	Rev 1

Manning roughness values

Channel markers were selected at the top of the channel banks for each cross section. The distance between the left and right channel markers varied as the channels progressed downstream, due to the steepness of the area.

Channel roughness values for the models were defined using Manning’s roughness coefficients “n”. Estimates of the range of Manning’s “n” were obtained from aerial photographs and based on Brisbane City Council Natural Channel Design Guidelines, December 2000. The aerial photographs show the channels to be well vegetated.

Table 3-34: Manning’ “n” Values

	High Manning’s “n”	Base Manning’s “n”	Low Manning’s “n”
Channel Bed	0.15	0.05	0.03
Channel Banks	0.15	0.15	0.1

Boundary conditions

The tail water level adopted for the HEC-RAS models was the 1 in 100 year ARI flood level of 2.6m, as detailed in the “Area E” – Terranora – Planning Report & Structure Plan for Terranora Landowners Group, (Jim Glazebrook & Associates Pty Ltd, 2002).

Flows

The flows calculated in XP-RAFTS for the developed scenario (without mitigation) were used in the HEC-RAS models. These flows were chosen as they will determine the worst case conditions in the channels.

The table below details the XP-RAFTS flows and where they were applied in the HEC-RAS models.

Table 3-35: Channel flows – developed

Channel	Max Flow (m ³ /s) from XP-RAFTS (1 in 100 yr ARI, 1 hr event)	HEC-RAS Reach/HEC-RAS chainage
Upstream JunctA-B	13.1	Reach 2 CH1500
JunctA-B - C	26.2	Reach 2 CH1200
C – D	38.8	Reach 2 CH850
F – G	53.3	Reach 2 CH450
Upstream H-I	7.2	Reach 2B CH850
H – I	14.3	Reach 2B CH650
JunctM-N - O	18.5	Reach 3 CH600

3.4.5.2 HEC-RAS results

The HEC-RAS models were run using the peak flows shown in Table 3.35. Flows, flood levels, velocities, flow areas and channel top widths are provided in the following tables.

Table 3-36: Q100 – base case HEC-RAS model results

Reach	Chainage	Flow (m3/s)	Min Channel Elev. (m)	Water Surface Elev. (m)	Max Channel Depth (m)	Channel Velocity (m/s)	Flow Area (m2)	Top Width (m)
2	1500	13.1	93.84	94.83	0.99	2.19	5.99	12.26
2	1450	13.1	89.49	90.55	1.06	2.23	5.87	11.56
2	1400	13.1	82.72	84.04	1.32	2.56	5.13	7.75
2	1350	13.1	76.96	78.21	1.25	2.48	5.29	8.46
2	1300	13.1	74.64	74.82	0.18	1.32	9.89	56.47
2	1250	13.1	67.89	68.94	1.05	2.31	5.68	9.06
2	1200	26.2	67.02	67.40	0.38	1.73	15.11	49.61
2	1150	26.2	60.58	61.60	1.02	2.43	10.77	17.91
2	1100	26.2	48.11	49.82	1.71	2.88	9.09	10.71
2	1050	26.2	41.88	43.44	1.56	2.87	9.14	10.98
2	1000	26.2	39.81	40.25	0.44	1.82	14.40	43.14
2	950	26.2	35.47	36.45	0.98	2.34	11.18	19.98
2	900	26.2	33.87	34.71	0.84	2.08	12.61	28.53
2	850	38.8	24.62	25.84	1.22	2.95	13.15	14.87
2	800	38.8	20.40	21.82	1.42	2.76	14.06	18.14
2	750	38.8	19.26	19.92	0.66	1.89	20.50	56.57
2	700	38.8	16.56	17.73	1.17	1.00	38.73	46.16
2	650	38.8	16.56	17.53	0.97	1.12	34.49	44.95
2	600	38.8	16.56	16.92	0.36	1.85	21.03	60.94
2	550	38.8	10.92	11.92	1.00	2.37	16.35	28.59
2	500	38.8	10.42	11.18	0.76	0.70	55.46	90.02
2	450	53.5	10.11	10.68	0.57	1.69	31.58	108.33
2	400	53.5	5.83	6.88	1.05	2.09	25.63	58.08
2	350	53.5	3.99	5.19	1.20	2.09	25.64	58.16
2	300	53.5	3.43	4.31	0.88	1.32	40.44	79.55
2	250	53.5	2.44	3.32	0.88	1.92	27.87	73.54
2	200	53.5	1.95	2.90	0.95	0.89	60.25	101.96
2	150	53.5	1.59	2.66	1.07	0.96	55.78	116.97
2	100	53.5	1.13	2.60	1.47	0.45	119.43	151.72
2	50	53.5	0.51	2.60	2.09	0.22	247.10	149.79
2B	850	7.2	108.92	109.75	1.91	1.92	3.76	9.96
2B	800	7.2	95.61	96.49	0.88	1.89	3.82	10.43
2B	750	7.2	87.04	88.10	1.06	2.28	3.16	5.97
2B	700	7.2	80.31	81.02	0.71	1.88	3.83	10.75
2B	650	14.3	71.16	72.44	1.28	2.09	6.86	15.91
2B	600	14.3	57.39	58.50	1.11	2.30	6.72	14.78
2B	550	14.3	44.49	45.68	1.19	2.26	6.34	12.27

Reach	Chainage	Flow (m3/s)	Min Channel Elev. (m)	Water Surface Elev. (m)	Max Channel Depth (m)	Channel Velocity (m/s)	Flow Area (m2)	Top Width (m)
2B	500	14.3	30.70	31.91	1.21	2.54	5.62	8.50
2B	450	14.3	15.61	16.39	0.78	2.27	6.29	11.98
2B	400	14.3	13.03	13.43	0.40	1.55	9.21	37.76
2B	350	14.3	8.99	9.41	0.42	1.33	10.72	59.07
2B	300	14.3	5.00	5.68	0.68	1.84	7.79	22.84
2B	250	14.3	3.18	3.72	0.54	1.50	9.55	41.69
2B	200	14.3	1.59	2.60	1.01	0.32	45.30	112.58
2B	150	14.3	1.39	2.60	1.21	0.11	131.13	128.84
2B	100	14.3	0.40	2.60	2.20	0.06	234.03	154.77
2B	50	14.3	0.00	2.60	2.60	0.04	408.11	191.66
3	600	18.5	32.92	33.59	1.97	1.98	9.36	23.71
3	550	18.5	17.60	18.78	1.18	2.55	7.24	10.91
3	500	18.5	13.03	14.05	1.02	2.26	8.18	15.68
3	450	18.5	9.71	10.25	0.54	2.16	8.56	17.88
3	400	18.5	7.38	8.04	0.66	1.92	9.63	25.83
3	350	18.5	6.15	6.37	0.22	1.17	15.87	73.52
3	300	18.5	4.00	4.74	0.74	2.16	8.55	18.06
3	250	18.5	1.87	2.58	0.71	0.96	19.35	65.59
3	200	18.5	1.24	2.60	1.36	0.14	136.89	152.27
3	150	18.5	0.62	2.60	1.98	0.06	326.31	223.35
3	100	18.5	0.25	2.60	2.35	0.04	486.70	267.12
3	50	18.5	0.11	2.60	2.49	0.03	614.35	289.06